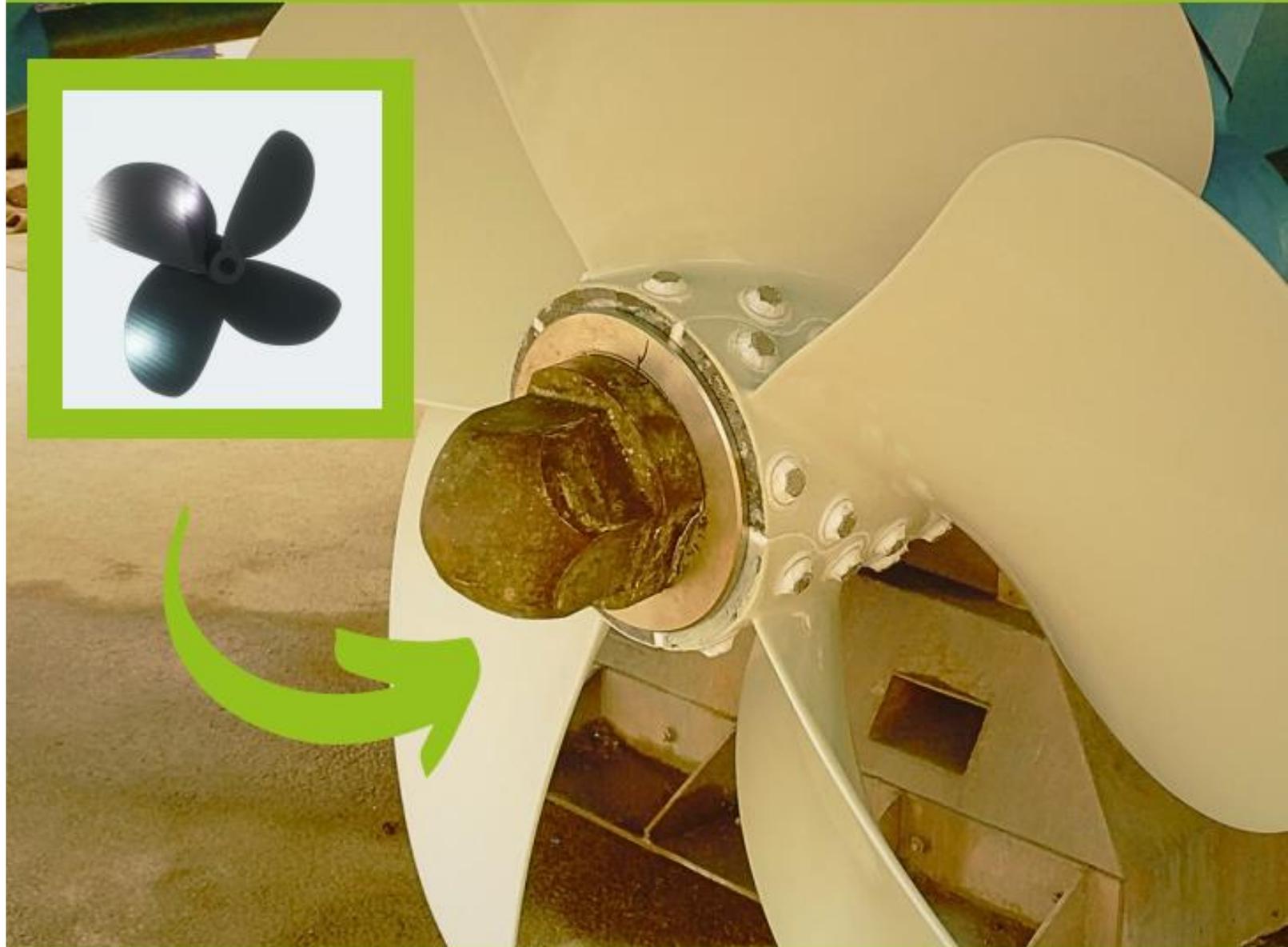


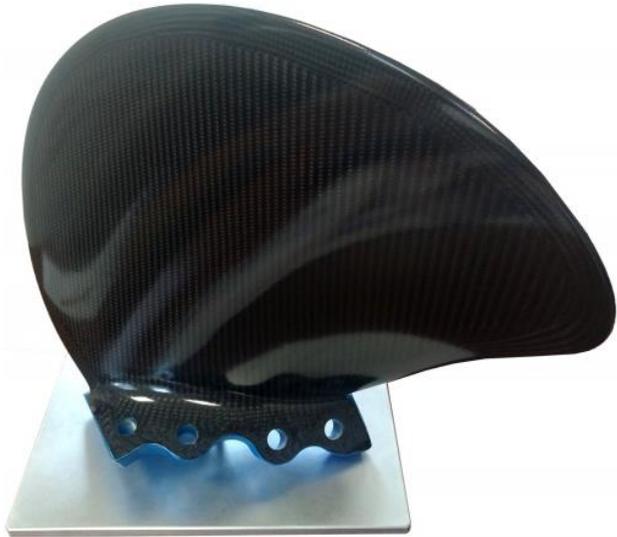
# **COPROPEL project: Composite propeller design considering fluid- structure interaction**

**E-Lass Seminar Day  
LAS PALMAS - 03/05/2023**

Marion LARREUR – Structural Engineer, MECA

Stéphane PABOEUF - Head of Composite Materials  
Section, Research Department, BUREAU VERITAS





## ***FABHELI project (2016 – 2018)***

*Loiretech, Méca, Naval Group + BV, AML*

*Proved the potential of using composite materials for propellers*

*Manufacturing with the RTM process*

*Validation in sea conditions*



- **Low vibration** : High damping performance absorbs vibration and reduces underwater radiated noise (URN)
- **Lightweight**: 50-60% lighter than current solutions
- **High performance**: Lower energy consumption creating a reduced environmental footprint
- **High Strength**: Improved reliability due to greater fatigue resistance

# CoPropel Project - Partners



BUREAU VERITAS



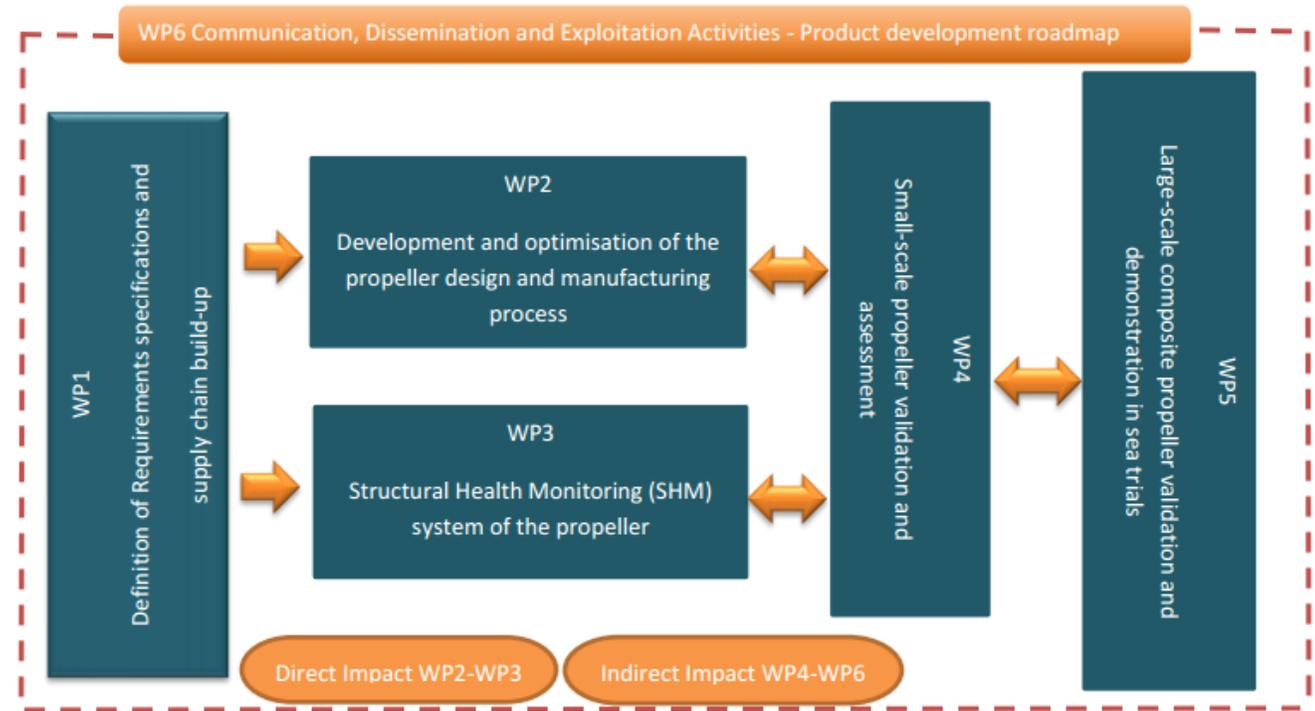
UNIVERSITY OF IOANNINA



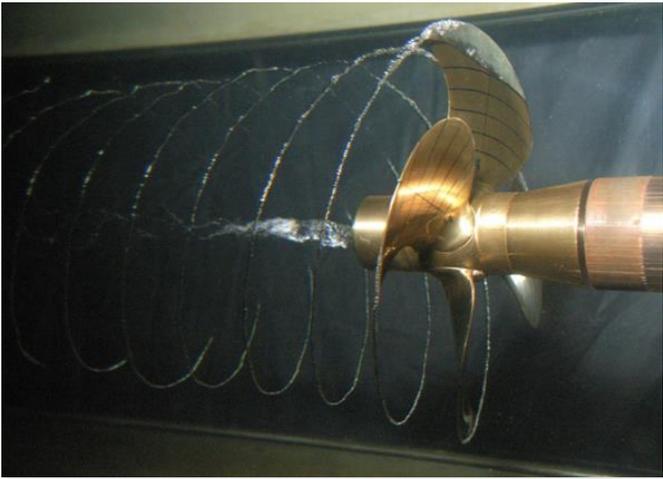
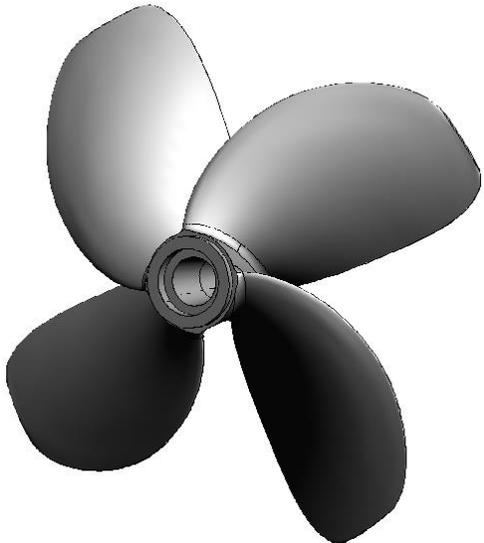
GLAFCOS MARINE



- **Design a composite propeller** to achieve optimum propulsive efficiency
- Optimize the **manufacturing process** based on closed mold resin infusion techniques
- Develop a **condition and structural health monitoring system** that will be embedded within the propeller
- Validation of the composite propeller with **small-scale and full-scale trials**
- Assist in the formulation of new **guidelines**
- **Communication and dissemination** of the project outcomes
- Define roll out strategy and develop a **business plan**



| <b>MADARA propeller (Danube river pusher)</b> |   |
|---|---|
| Number of engines                             | 2   |
| Number of propellers                          | 2 ( <i>symmetrical</i> )  |
| Number of blades                              | 4   |
| Diameter of the propellers                    | 1 960 mm ( <i>full-scale</i> )<br>250 mm ( <i>small-scale tests</i> ) |



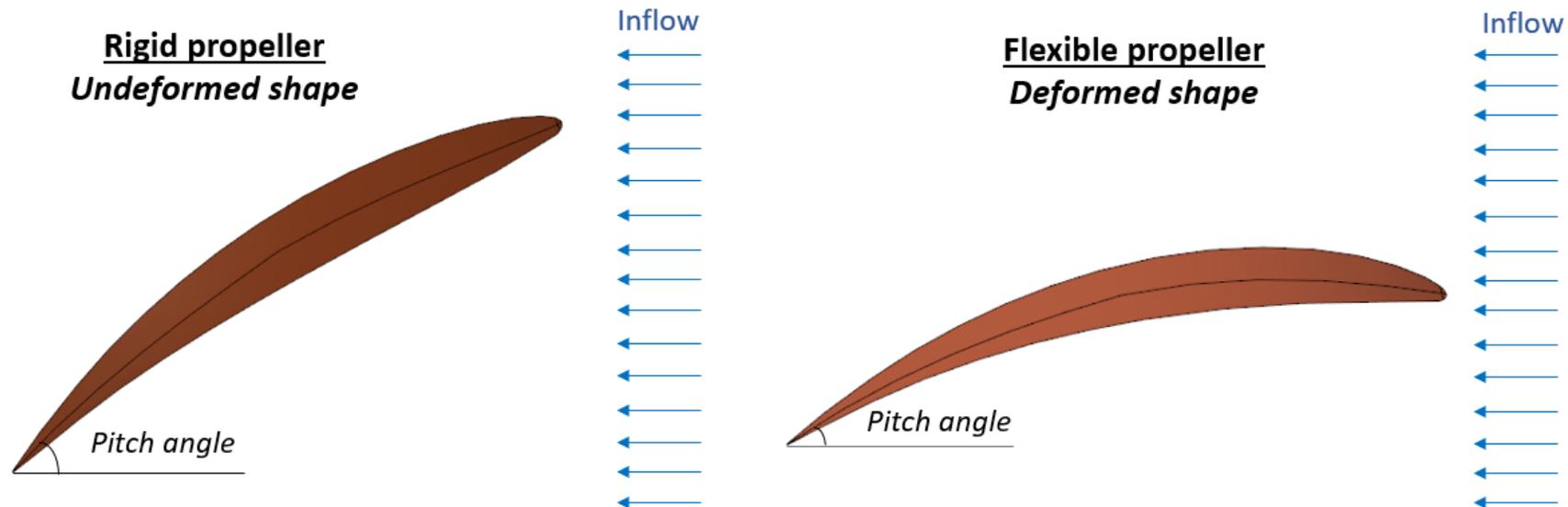
Metallic propeller (rigid) : optimal for **one operating condition**

Composite propeller (flexible) : orientation of the blade profile adapts with the changing flow, increased efficiency over **a range of operating conditions**

Technology based on **bend-twist coupling** characteristic of composites

Anisotropy of the propeller created by the **optimization of the stacking angles** for expected loads

Difference of deflection between the trailing edge and the leading edge, the **pitch changes with loading**



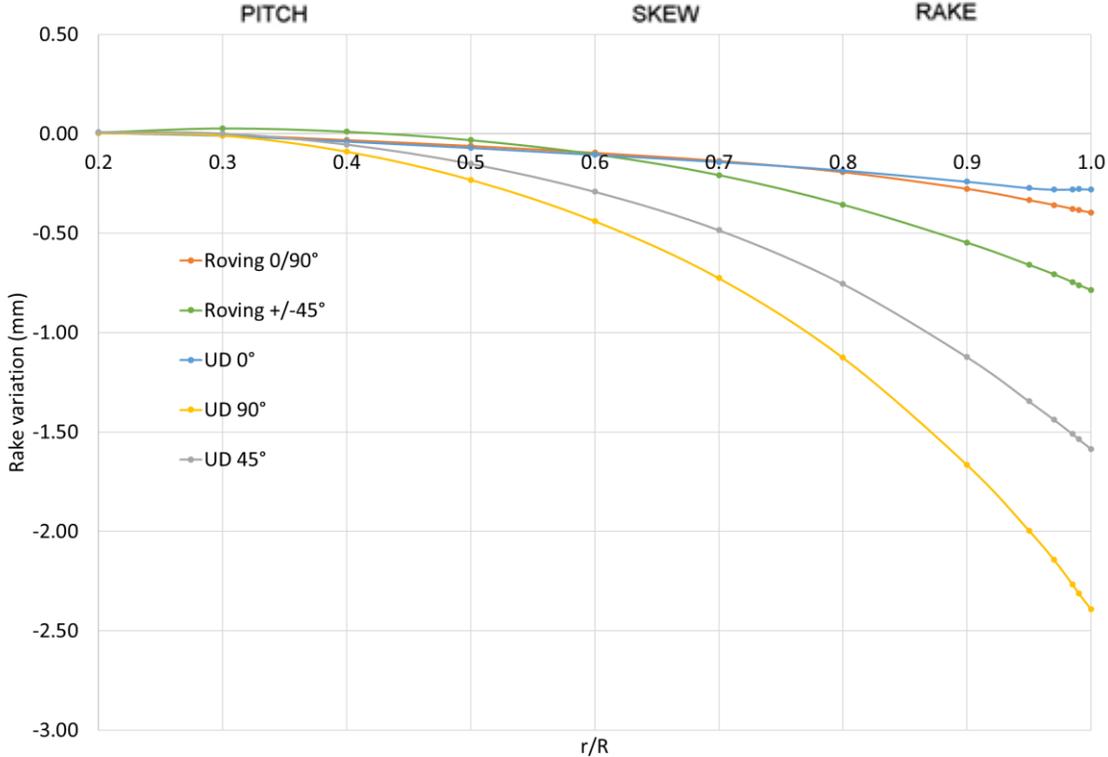
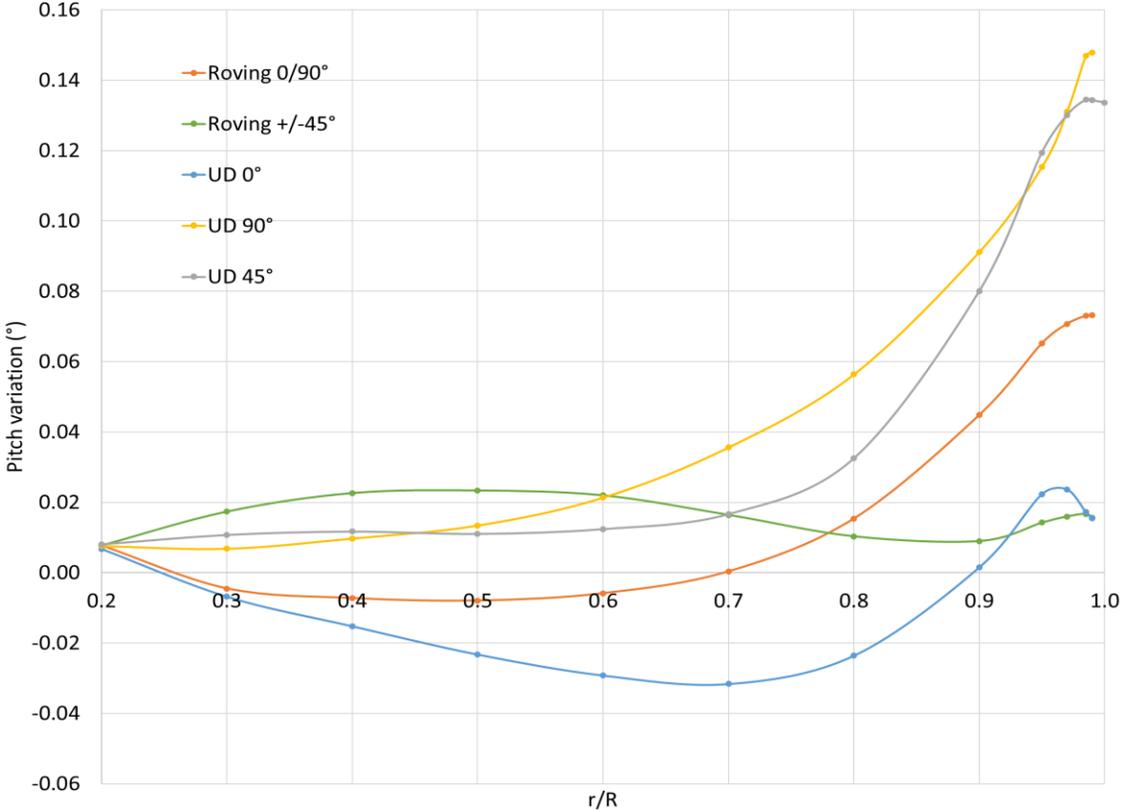
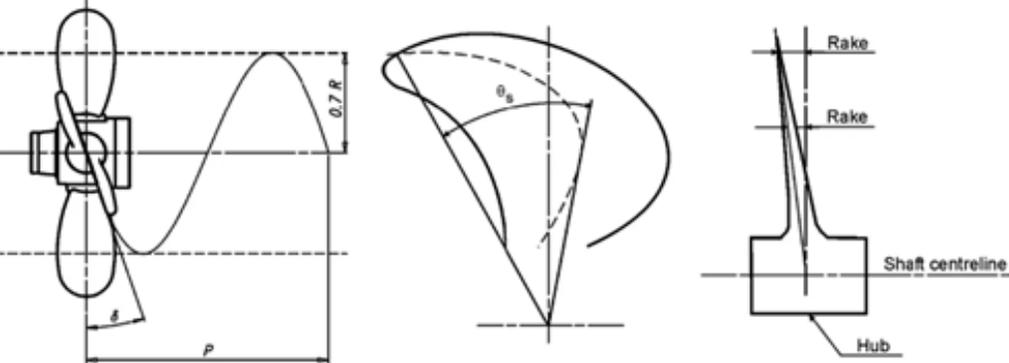
# Flexibility of composite propeller



Example – Influence of fiber orientation on a 3D homogeneous model of the small-scale Madara blade

*Carbon fiber / epoxy resin*

*0° direction = reference line of the blade*

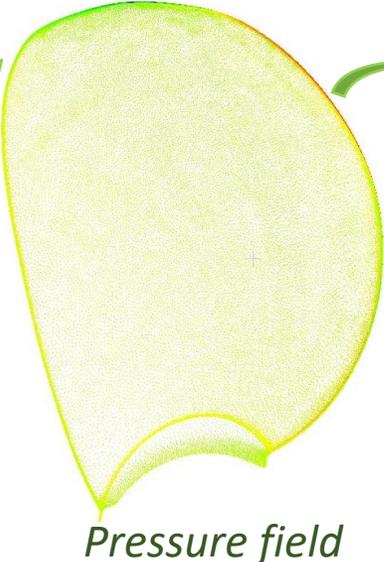
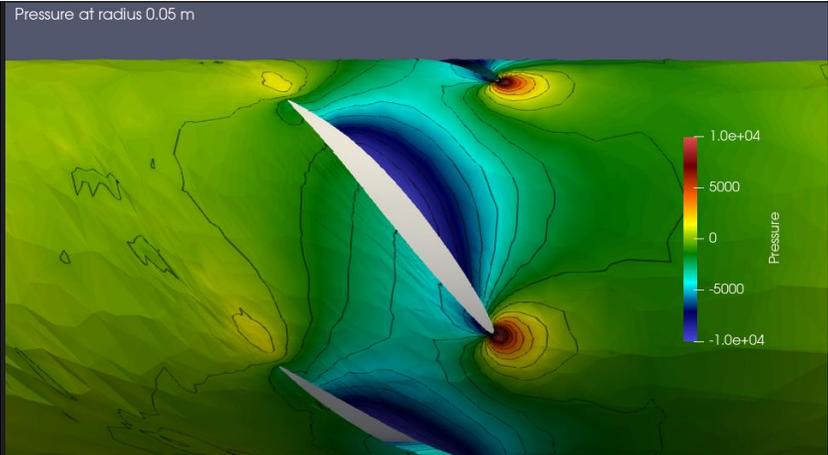




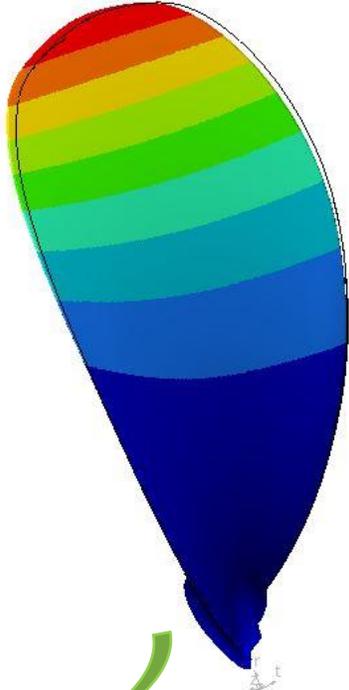
Deformation of composite propeller under fluid loads influences the hydrodynamic performance

*Need to develop representative structural and hydrodynamic models for design, that allow the transfer of data*

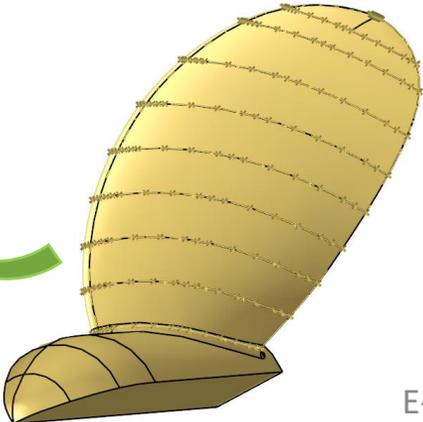
CFD calculation



FEM calculation

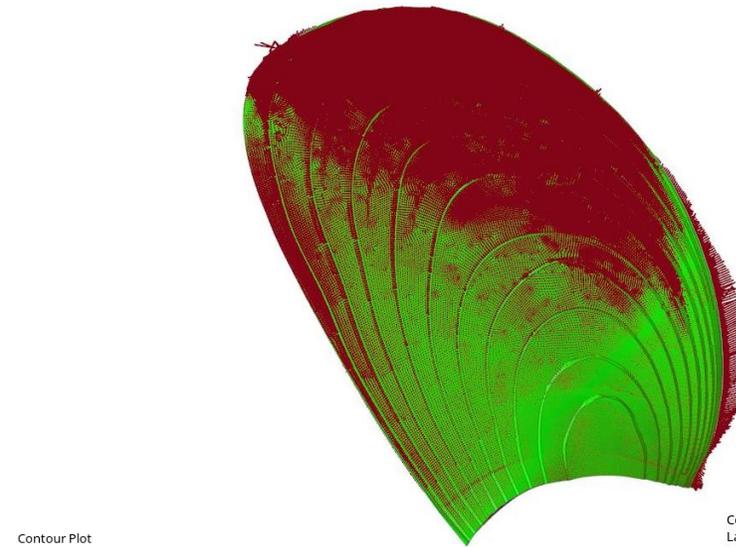


Deformed shape



| r/R   | r      | Pitch   | C      | C_LE   | P_angle | tmax  | RAKE  |
|-------|--------|---------|--------|--------|---------|-------|-------|
| -     | mm     | mm      | mm     | mm     | deg     | mm    | mm    |
| 0.20  | 199.00 | 1145.00 | 524.10 | 321.90 | 42.48   | 71.50 | 20.00 |
| 0.30  | 298.50 | 1231.00 | 595.30 | 364.70 | 33.28   | 64.20 | 30.00 |
| 0.40  | 398.00 | 1300.00 | 648.60 | 390.20 | 27.47   | 55.80 | 40.00 |
| 0.50  | 497.50 | 1346.00 | 681.50 | 399.00 | 23.30   | 47.50 | 50.00 |
| 0.60  | 597.00 | 1376.00 | 692.70 | 388.50 | 20.14   | 39.20 | 60.00 |
| 0.70  | 696.50 | 1379.00 | 681.50 | 356.10 | 17.49   | 30.90 | 70.00 |
| 0.80  | 796.00 | 1365.00 | 623.50 | 288.50 | 15.27   | 22.20 | 80.00 |
| 0.90  | 895.50 | 1329.00 | 510.40 | 181.50 | 13.29   | 13.80 | 90.00 |
| 0.95  | 945.25 | 1302.00 | 411.90 | 104.10 | 12.36   | 10.10 | 95.00 |
| 0.97  | 965.15 | 1290.00 | 349.00 | 59.20  | 12.01   | 8.50  | 97.00 |
| 0.985 | 980.08 | 1285.00 | 256.00 | 15.00  | 11.82   | 7.40  | 98.50 |

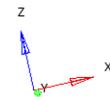
- Thickness discretization, ply drop-off
- Blade deformation control
- Multi-layers approach
- Ply-by-ply stresses, strain evaluation
- Verification of criteria with BV rules
- Parametrized model for optimization
- Integration of SHM system, assembly to the hub, manufacturing limitations
- Frequency calculation in water
- Validation with small-scale and full-scale testing



Contour Plot  
Displacement(Mag)  
Analysis system

|           |
|-----------|
| 4.425E-01 |
| 3.933E-01 |
| 3.442E-01 |
| 2.950E-01 |
| 2.458E-01 |
| 1.967E-01 |
| 1.475E-01 |
| 9.833E-02 |
| 4.916E-02 |
| 0.000E+00 |
| No Result |

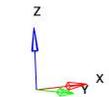
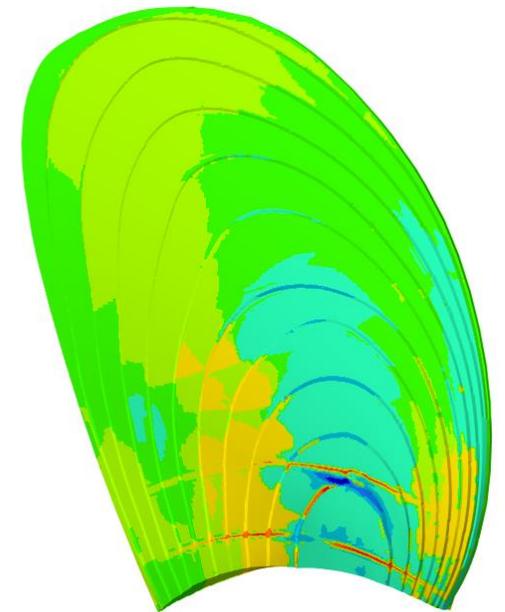
Max = 4.425E-01  
Grids 1380009  
Min = 0.000E+00  
Grids 1316302



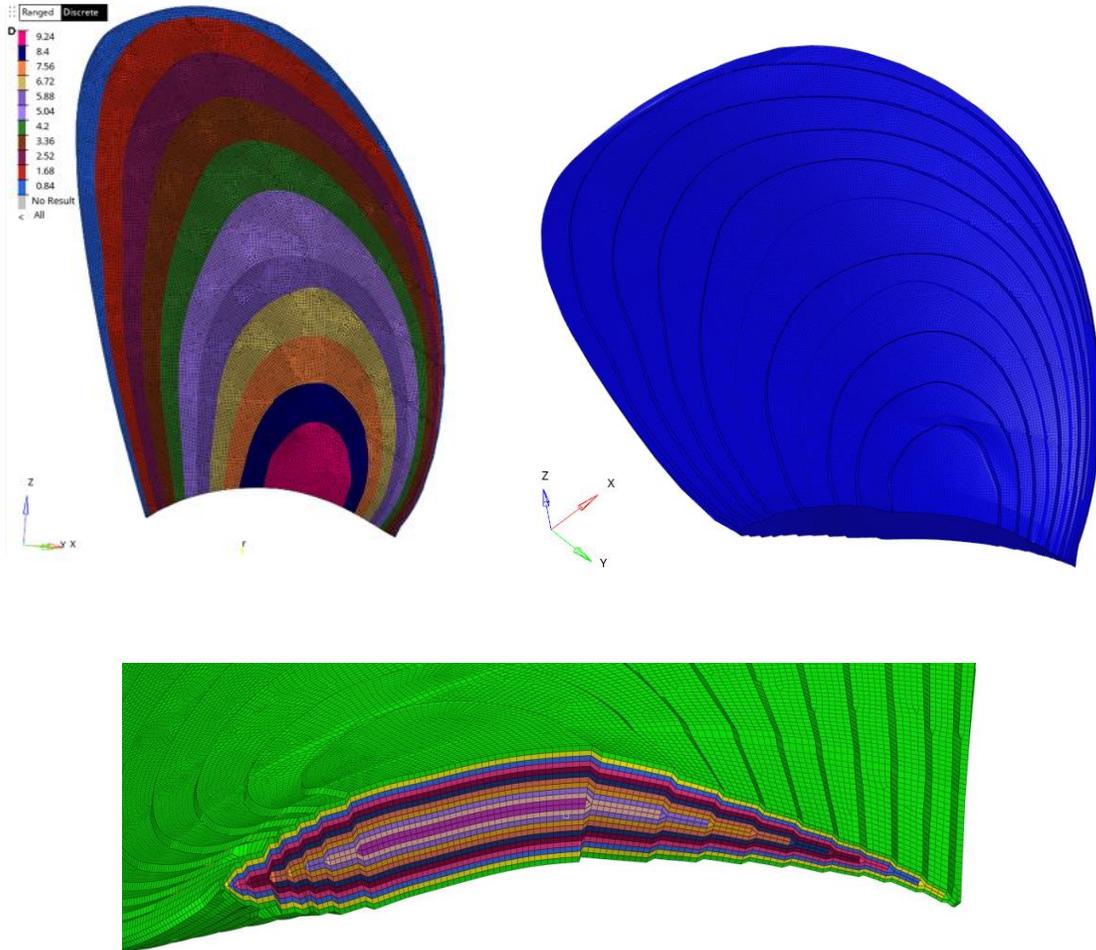
Contour Plot  
Layered Solid Failure Index (Hoffman)(Failure Index, Extreme)  
Simple Average

|            |
|------------|
| 2.926E-02  |
| 2.197E-02  |
| 1.469E-02  |
| 7.397E-03  |
| 1.088E-04  |
| -7.180E-03 |
| -1.447E-02 |
| -2.176E-02 |
| -2.905E-02 |
| -3.633E-02 |
| No Result  |

Max = 2.926E-02  
Node 1400397  
Min = -3.633E-02  
Node 1399682



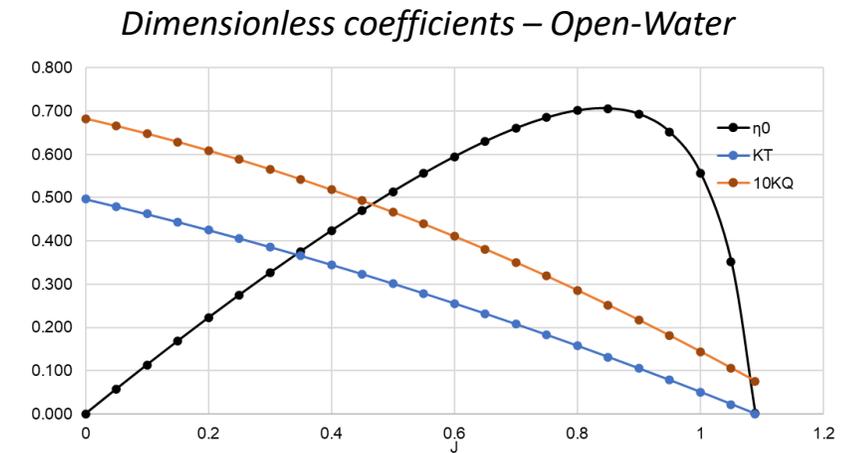
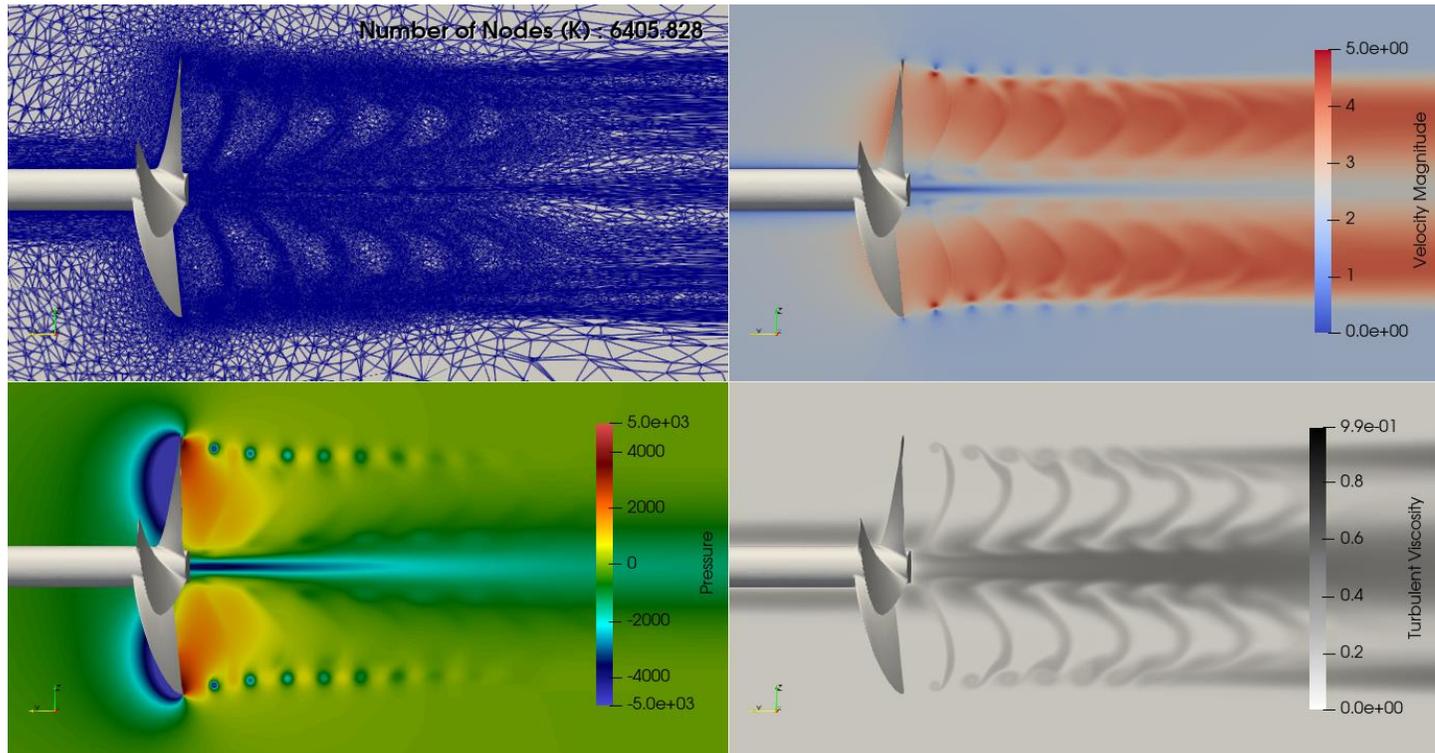
## Benchmark of element types



| Model type   | 2D multilayer shell | 3D Solid with homogeneous properties | 3D Solid Laminate 1EL in thickness | 3D Solid Laminate >1EL in thickness |
|--|---------------------|--------------------------------------|------------------------------------|-------------------------------------|
| <i>Reliability of the results (FE formulation)</i> | --                  | -                                    | +                                  | +                                   |
| <i>Time to develop model and meshing</i>           | ++                  | +                                    | -                                  | -                                   |
| <i>Load application – data transfer with CFD</i>   | -                   | +                                    | +                                  | +                                   |
| <i>Calculation time</i>                            | ++                  | +                                    | -                                  | --                                  |
| <i>Material orientation</i>                        | +                   | -                                    | -                                  | -                                   |
| <i>Modification of the stacking sequence</i>       | ++                  | -                                    | +                                  | -                                   |
| <i>Failure criterion, type of outputs</i>          | +                   | --                                   | +                                  | +                                   |
| <i>Visual validation</i>                           | ++                  | -                                    | +                                  | ++                                  |

- Performance evaluation
- Load pressure distribution
- Computation of thrust, torque and efficiency

- Adaptive meshing software, convergence study
- Influence of the hull
- Validation with experiments and other calculation methods



- Advance ratio:  $J = V_a / (nD_p)$
- Thrust coefficient:  $K_T = T / (\rho n^2 D_p^4)$
- Torque coefficient:  $K_Q = Q / (\rho n^2 D_p^5)$
- Efficiency :  $\eta_0 = JK_T / (2\pi K_Q)$

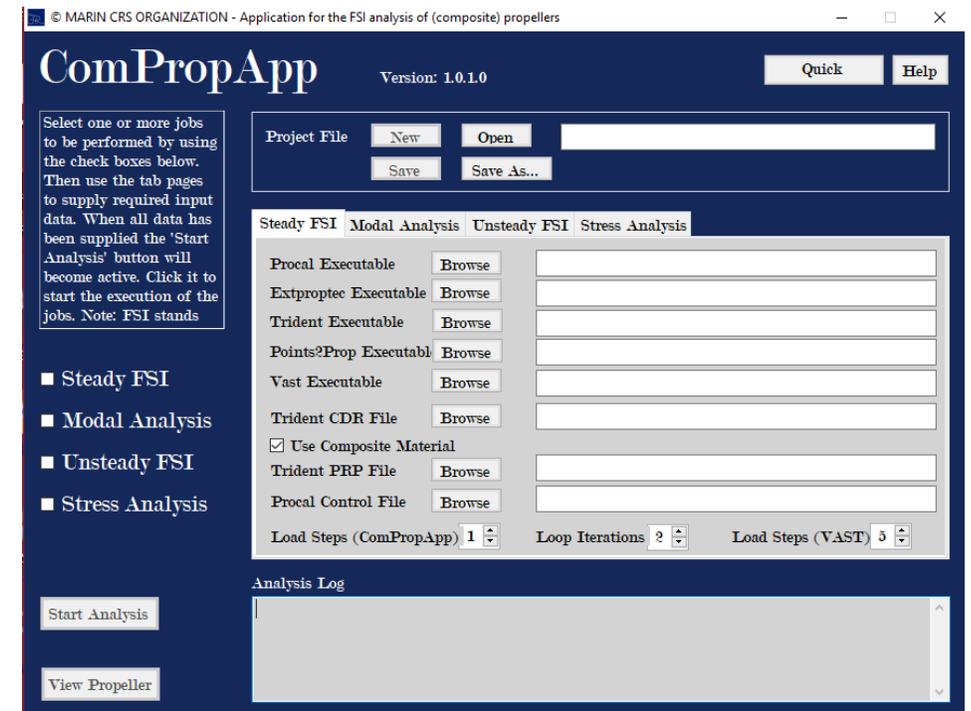
# ComPropApp – Hydro-Structure coupling

**ComPropApp**, a Fluid-Structure Interaction tool for flexible propeller

- Developed within Comprop & Comprop2 and ORCA projects
- Cooperative Research Ship (CRS), organisation led by 

## Coupling of:

- Fluid model: Boundary Element Method (BEM)
  - ➔ Procal
    - Inviscid/Isovolume/Irrotational fluid flow
- Structural model: Finite Element Model (FEM)
  - ➔ Trident/VAST solvers
    - Homogenized anisotropic materials properties



## Validation of ComPropApp: 4 methods investigated

| 1  | 2   | 3   | 4   |
|--|---|---|---|
| <b>BEM-FEM</b><br>One-way                                      | <b>BEM-FEM</b><br>One-way   | <b>RANS-FEM</b><br>One-way  | <b>RANS-FEM</b><br>Two-way  |
| <ul style="list-style-type: none"> <li>• ComPropApp</li> </ul> | <ul style="list-style-type: none"> <li>• Procal</li> <li>• FEMAP &amp; Nastran</li> </ul> | <ul style="list-style-type: none"> <li>• StarCCM+</li> <li>• FEMAP &amp; Nastran</li> </ul> | <ul style="list-style-type: none"> <li>• StarCCM+</li> <li>• FEMAP &amp; Nastran</li> </ul> |

### Application case: FabHeli Propeller<sup>(1)</sup>

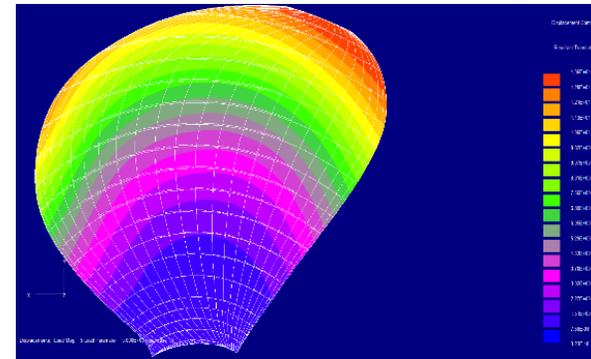
- Diameter: 1.10 m
- Number of blades: 5
- Materials: Carbon fibres
- Process: RTM (Resin Transfer Molding)
- Connection to the hub: Bolted



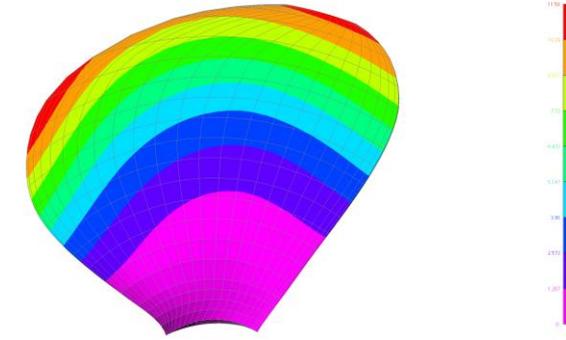
<sup>(1)</sup> **FabHeli: French research project (2017-2020)**  
DGA (French Department of Defense), LoireTech, Meca, Naval Group, AML, BV

## Comparison of results

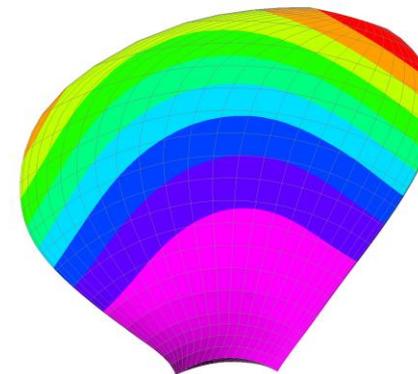
| 1   | 2                             | 3                               | 4                               |
|---|-------------------------------|---------------------------------|---------------------------------|
| <b>BEM-FEM</b><br>One-way                           | <b>BEM-FEM</b><br>One-way     | <b>RANS-FEM</b><br>One-way      | <b>RANS-FEM</b><br>Two-way      |
| • ComPropApp  | • Procal<br>• FEMAP & Nastran | • StarCCM+<br>• FEMAP & Nastran | • StarCCM+<br>• FEMAP & Nastran |
| <b>Thrust</b>                                       | <b>0%</b>                     | <b>1.08%</b>                    | <b>-0.44%</b>                   |
| <b>Torque</b>                                       | 0%                            | -0.91%                          | -2.07%                          |
| <b>Max. displ.</b>                                  | -14.85%                       | -4.93%                          | -6.32%                          |
| <b><i>Difference with Method 1 - ComPropApp</i></b> |                               |                                 |                                 |



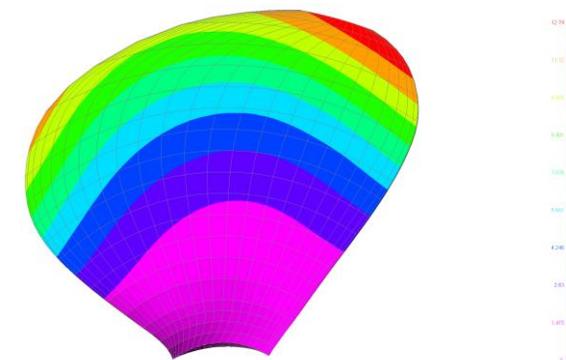
Method 1: max displacement 13.6 mm



Method 2: max displacement 11.58mm



Method 3: max displacement 12.93 mm



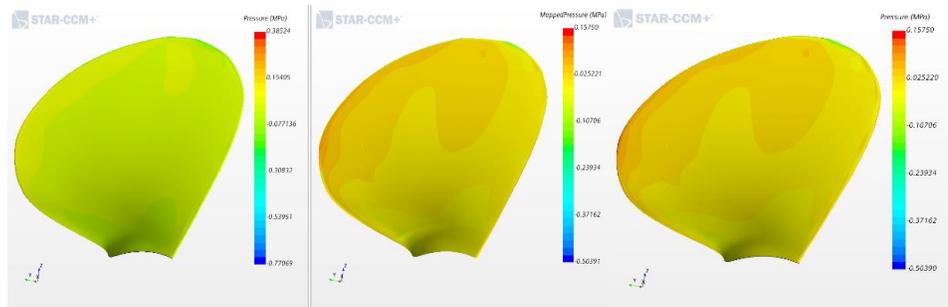
Method 4: max displacement 12.74 mm

Paboeuf et al, *Validation of a Fluid Structure Interaction Tool for Flexible Propeller in Composite Materials*, Proceedings of the PRADS 2022 Conference, Dubrovnik, Croatia, October 2022.

## Analysis of results

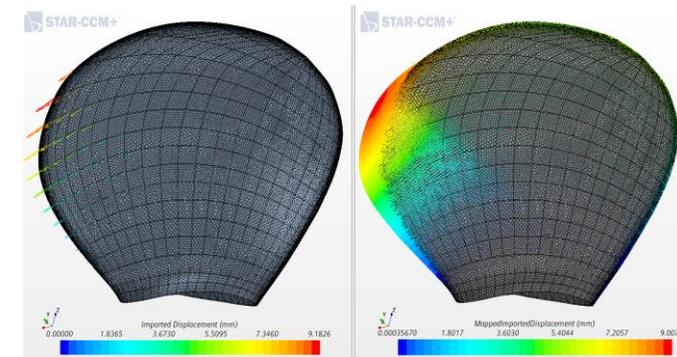
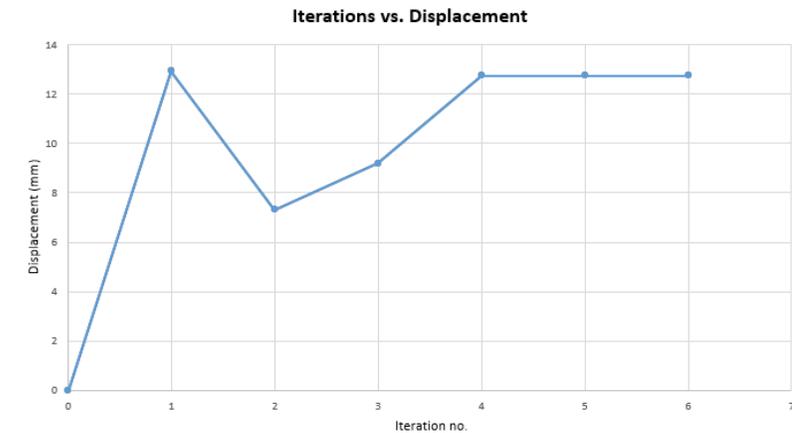
### Method 4 – RANS-FEM Two-way

- **Pressure and displacement field mapping**
  - StarCCM+ to FEMAP **AND** FEMAP to StarCCM+
  - Fine to coarse mesh **AND** coarse to fine mesh
- **Pressure loss at leading edge → No significant effect**

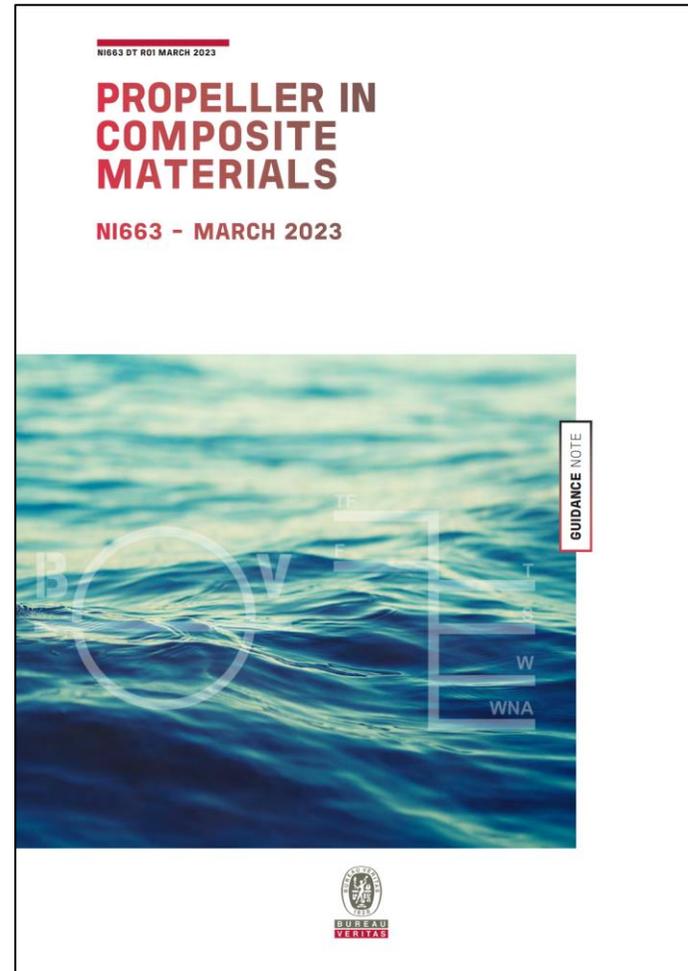
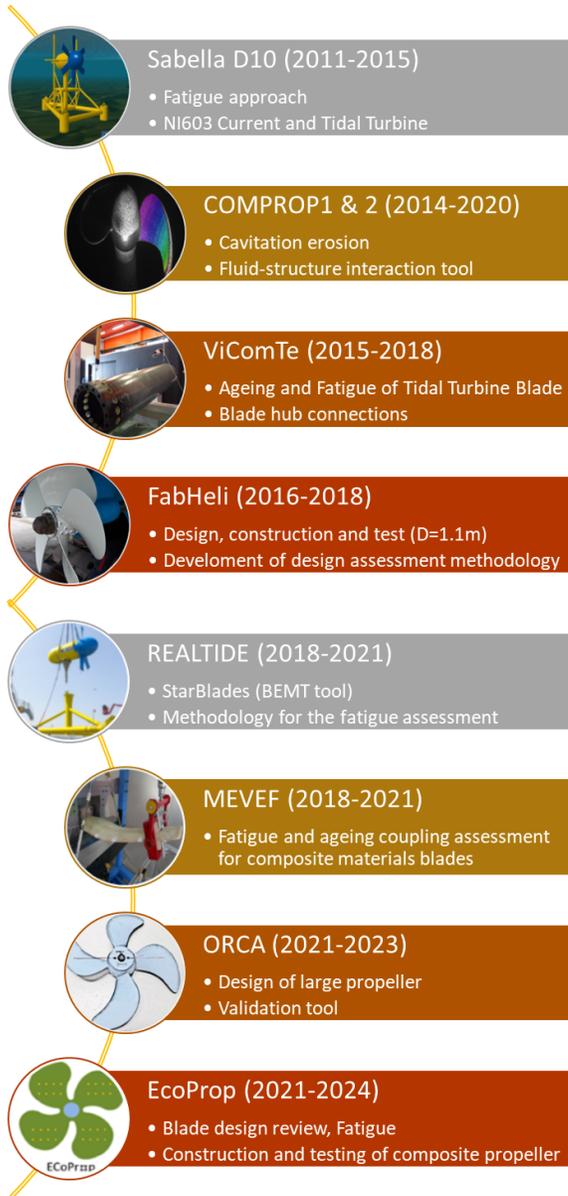


- **Displacement field mapping → Small percentage of discrepancy**

| 1                         | 2                             | 3                               | 4                               |
|---------------------------|-------------------------------|---------------------------------|---------------------------------|
| <b>BEM-FEM</b><br>One-way | <b>BEM-FEM</b><br>One-way     | <b>RANS-FEM</b><br>One-way      | <b>RANS-FEM</b><br>Two-way      |
| • ComPropApp              | • Procal<br>• FEMAP & Nastran | • StarCCM+<br>• FEMAP & Nastran | • StarCCM+<br>• FEMAP & Nastran |



# NI663 Propeller in Composite Materials



## BV Guidance Note for propellers made in Composite Materials covering:

- Process of certification
  - Design Phase
  - Production Phase
- Design assessment
  - Analytical
  - Numerical
- Testing
  - Coupons
  - Prototype
- Manufacturing
- In-service surveys
  - Periodic survey
  - NDT

- ***Use of composite propellers and optimization of the stacking sequence to improve efficiency***
- ***Design of shape adaptative structure involving two-way fluid-structure interaction (FEM - CFD)***
- ***Development of accurate and efficient structural and hydrodynamical models***
- ***Alternative numerical method for hydro-structure coupling with ComPropApp***
- ***Roadmap for the certification of composite propellers and improvements of NI663***





# Thank you for your attention!

## Any questions?

>> **Contact:**

Marion Larreur / MECA / [marion.larreur@calcul-meca.fr](mailto:marion.larreur@calcul-meca.fr)

Stéphane Paboeuf / Bureau Veritas / [stephane.paboeuf@bureauveritas.com](mailto:stephane.paboeuf@bureauveritas.com)

# Composite propeller design

## General assumptions - Material properties

The mechanical characteristics of raw materials (fiber and resin) are taken from BV NR546 for certification purpose, according to NI663.

|                                 |                   | <b>BV Carbon HS</b> | <i>Toray T300</i> |
|---------------------------------|-------------------|---------------------|-------------------|
| <i>Density</i>                  | kg/m <sup>3</sup> | 1880                | 1760              |
| <i>Tensile modulus</i>          | MPa               | 238000              | 230000            |
| <i>Axial Poisson ratio</i>      | -                 | 0.3                 | /                 |
| <i>Transverse Young modulus</i> | MPa               | 15000               | /                 |
| <i>Transverse Poisson ratio</i> | -                 | 0.02                | /                 |
| <i>Shear modulus</i>            | MPa               | 50000               | /                 |
| <i>Tensile strength</i>         | MPa               | 3600                | 3530              |
| <i>Compressive strength</i>     | MPa               | 2140                | /                 |
| <i>Shear strength</i>           | MPa               | 1200                | /                 |

|                                     |                   | <b>BV Epoxy</b> | <i>Sicommin SR8100</i> |
|-------------------------------------|-------------------|-----------------|------------------------|
| <i>Density</i>                      | kg/m <sup>3</sup> | 1250            | 1158                   |
| <i>Glass Transition Temperature</i> | °C                | 80 - 150        | 63 - 88                |
| <i>Tensile modulus</i>              | MPa               | 3100            | 2800 - 3200            |
| <i>Poisson ratio</i>                | -                 | 0.39            | /                      |
| <i>Shear modulus</i>                | MPa               | 1500            | /                      |
| <i>Tensile strength</i>             | MPa               | 75              | 50 - 71                |
| <i>Compressive strength</i>         | MPa               | 75              | /                      |
| <i>Shear strength</i>               | MPa               | 80              | 41 - 47                |

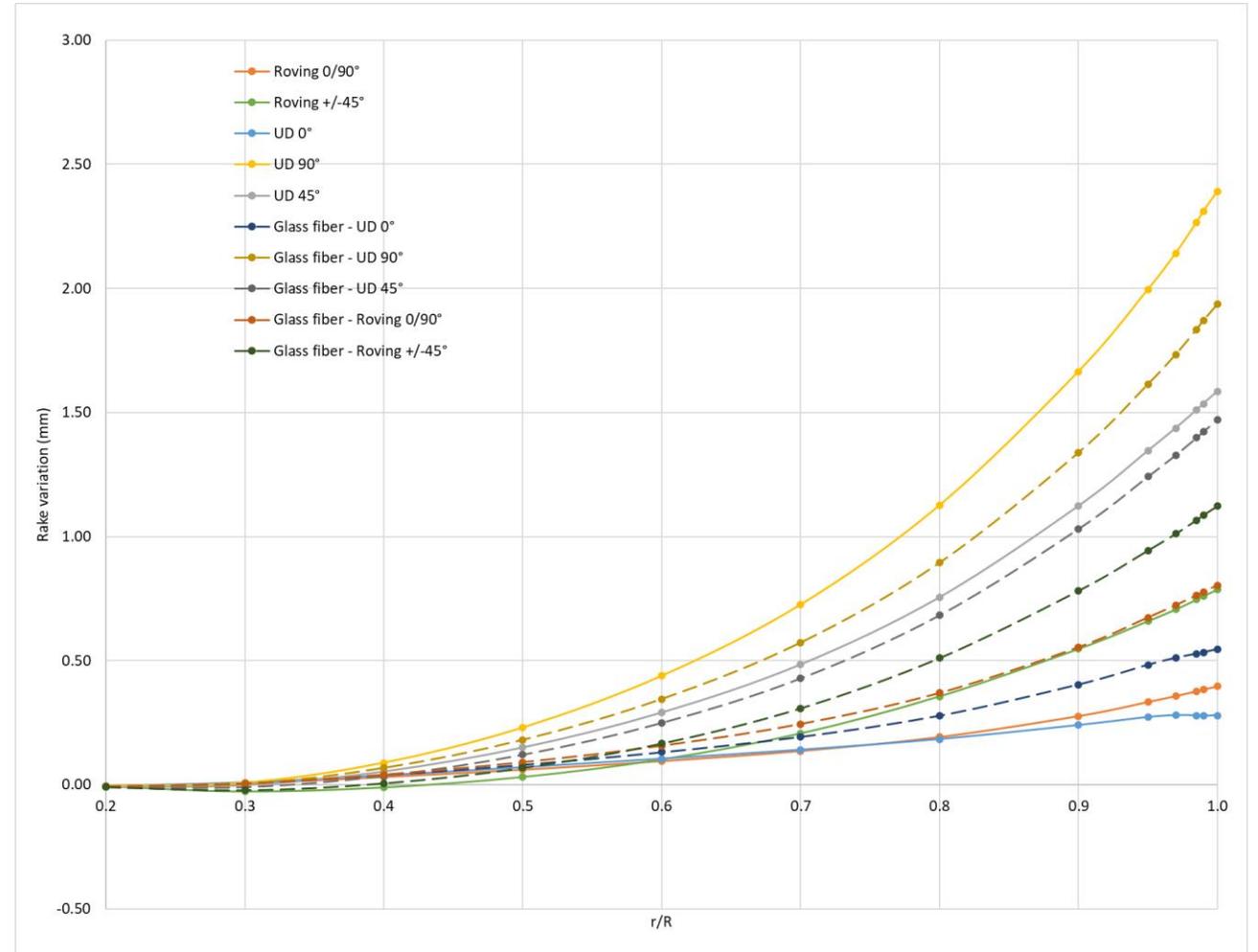
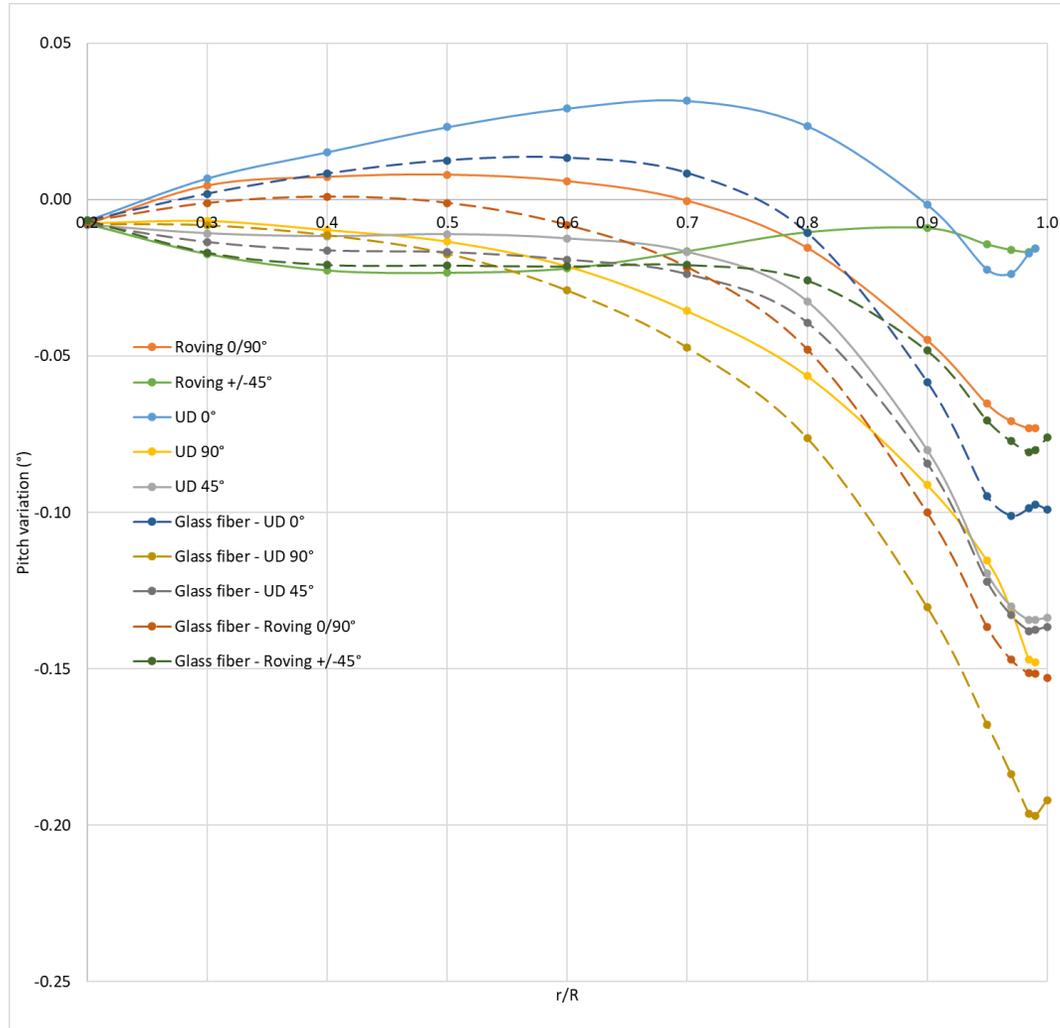
Material properties are to be considered layer by layer according to NR546 requirements. The fiber volume fraction is considered to be 40% (LRT).

|   |                   | <b>Unidirectional</b> | <b>Twill 2-2</b> |
|---|-------------------|-----------------------|------------------|
| <i>Fiber mass fraction</i>              | -                 | 49.3%                 | 49.3%            |
| <i>Volume fiber fraction</i>            | -                 | 40.0%                 | 40.0%            |
| <i>Density</i>                          | kg/m <sup>3</sup> | 1454                  | 1454             |
| <i>Thickness for 100g/m<sup>2</sup></i> | g/m <sup>2</sup>  | 0.140                 | 0.140            |
| <b>Stiffness</b>                        |                   |                       |                  |
| <i>Young Modulus X</i>                  | MPa               | 97118                 | 51087            |
| <i>Young Modulus Y</i>                  | MPa               | 4734                  | 51087            |
| <i>Young Modulus Z</i>                  | MPa               | 4734                  | 4734             |
| <i>Shear Modulus XY</i>                 | MPa               | 2984                  | 2984             |
| <i>Shear Modulus XZ</i>                 | MPa               | 2984                  | 2686             |
| <i>Shear Modulus YZ</i>                 | MPa               | 2089                  | 2686             |
| <i>Poisson Ratio XY</i>                 | -                 | 0.280                 | 0.026            |
| <i>Poisson Ratio XZ</i>                 | -                 | 0.280                 | 0.235            |
| <i>Poisson Ratio YZ</i>                 | -                 | 0.190                 | 0.235            |
| <b>Strength</b>                         |                   |                       |                  |
| <i>Tensile strength X</i>               | MPa               | 1165                  | 511              |
| <i>Compressive strength X</i>           | MPa               | 971                   | 511              |
| <i>Tensile strength Y</i>               | MPa               | 40                    | 434              |
| <i>Compressive strength Y</i>           | MPa               | 109                   | 434              |
| <i>Tensile strength Z</i>               | MPa               | 40                    | 434              |
| <i>Compressive strength Z</i>           | MPa               | 109                   | 434              |
| <i>Shear strength XY</i>                | MPa               | 48                    | 46               |
| <i>Shear strength XZ</i>                | MPa               | 48                    | 42               |
| <i>Shear strength YZ</i>                | MPa               | 40                    | 42               |

*NI663: Mechanical tests will be performed on test panels representative of the scantling and the manufacturing process used for the propeller manufacturing, and compared with theoretical properties.*

# Composite propeller design

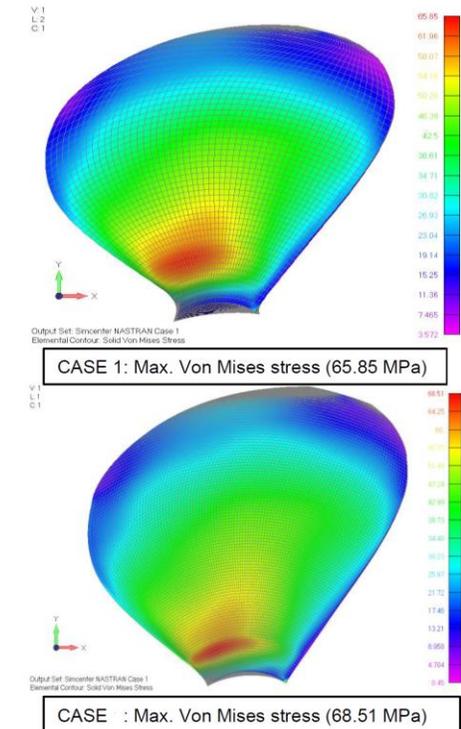
## Comparison of deformed shape obtained with carbon and glass fibers



## Analysis of results

### Isotropic materials

|                             | ISOTROPIC STEEL BLADE CASE                               |   |   |  | Relative Difference |                 |
|-----------------------------|--|---|---|--|---------------------|-----------------|
|                             | 1. BEM-FEM one-way coupled FSI Analysis (PROCAL & FEMAP) | 2. RANSE-FEM one-way coupled FSI Analysis (STAR-CCM+ & FEMAP) | 3. BEM-FEM explicit two-way coupled FSI Analysis (ComPropApp) | 4. RANSE-FEM strong two-way coupled FSI Analysis (STAR-CCM+) | CASE 1 & CASE 2     | CASE 3 & CASE 4 |
| Thrust (N)                  | CASE 1   | CASE 2  | CASE 3  | CASE 4   | CASE 1 & CASE 2     | CASE 3 & CASE 4 |
| Thrust (N)                  | 50,720   | 49,195  | 50,160  | 49,420   | 3.10%               | 1.5%            |
| Torque (N.m)                | 10,673   | 10,220  | 10,372  | 10,280   | 4.43%               | 0.90%           |
| Max. displacement (mm)      | 1.789  | 1.798   | 1.7   | 1.875  | -0.5%               | -9.33%          |
| Max. Von Mises stress (MPa) | 65.85  | 68.51   | 65.7  | 66.5   | -3.88%              | -1.2%           |



Rehman W. et al, *A comparison of different fluid-structure interaction analysis techniques for the marine propeller*, Proceedings of the ASME 2021 Power Conference, Online, July 2021.

## Analysis of results

|   | Pre-processing | Computation | Post-processing | Total Time | Processor     | Number of cores | RAM   |
|---|----------------|-------------|-----------------|------------|---------------|-----------------|-------|
| <b>1</b>  |                |             |                 |            |               |                 |       |
| <b>BEM-FEM</b><br>One-way<br><br>• ComPropApp                     | 4 hours        | 30 mins     | 10 mins         | ≈5 hours   | Intel i7      | 4 cores         | 16 GB |
| <b>4</b>  |                |             |                 |            |               |                 |       |
| <b>RANS-FEM</b><br>Two-way<br><br>• StarCCM+<br>• FEMAP & Nastran | 5 days         | 6 hours     | 10 hours        | ≈7 days    | Linux cluster | 112 cores       | 60 GB |