

**E-LASS Conference**  
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**DESIGN OF CAR DECKS WITH  
COMPOSITE PANELS INTRODUCED  
ON A 7000 CARS CAR CARRIER**



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- Introduction
- Background
- Design
  - Rules and regulation requirements
  - Additional assesment
- Production
- Conclusion
- Follow up projects

# Introduction

Why composites?



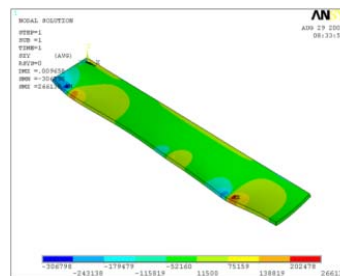
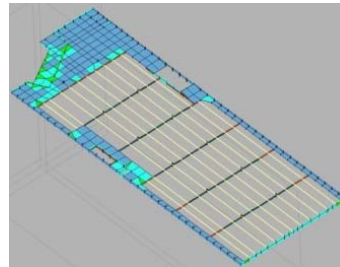
# Background



**DELIGHT TRANSPORT - Cargo deck of composite materials for RO-RO vessels**  
(FP6-031483, 2006-2010)

## DESIGN OPTIMISATION , PROTOTYPE AND TESTING

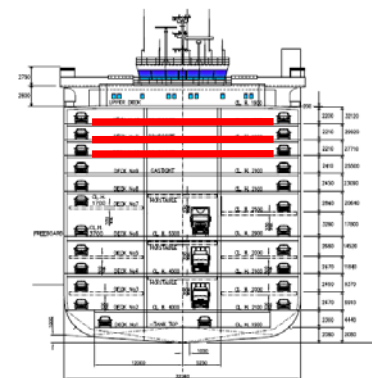
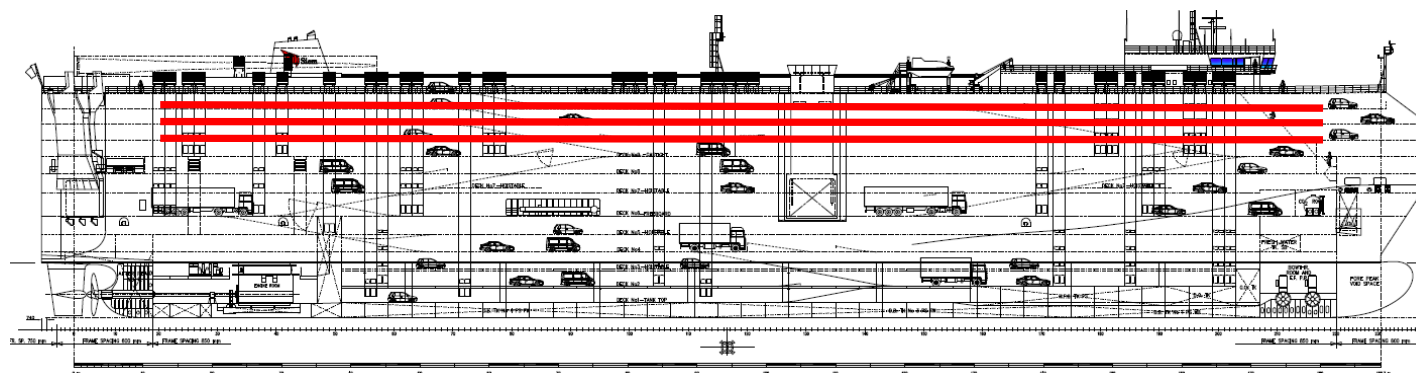
- Deck structure weight reduction up to 35%
- Fuel consumption reduction up to 2% → CO<sub>2</sub> emission reduction
- Total Lifecycle operation cost savings
- Production process cost reduction
- Satisfactory test results





# „Composite decks” on a SOLAS vessel

## Car carrier - 7000 cars



### MAIN PARTICULARS :

LENGTH overall	max. 200.00	m
LENGTH b.p.	188.70	m
BREADTH moulded	32.26	m
DEPTH to upper deck moulded	32.12	m
DRAUGHT design	8.00	m
DRAUGHT scantling	8.80	m
DEADWEIGHT at design draught	13 370	t
DEADWEIGHT at scantling draught	17 170	t
MAIN ENGINE	M.A.N. – B & W – ULJANIK 7 S 50 ME-B9.5	
OUTPUT MCR	11 200 kW / 117 r.p.m.	
SPEED trial ( 9520 kW at draught design )	19.7	knots

Classification society: **Bureau Veritas**

Flag: **Liberia**



# Design procedure

Requirements:

- Owner
- Class
- SOLAS
  - Construction
  - Fire safety

→ Conventional or Alternative design procedure ?

# „Composite decks” on a SOLAS vessel

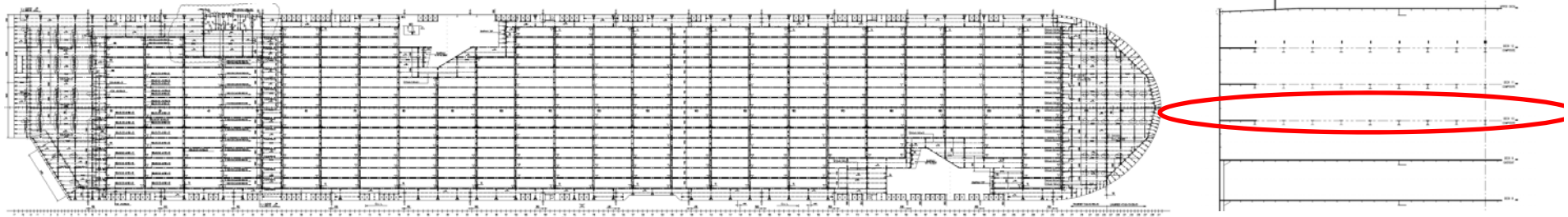
## SOLAS - CONSTRUCTION

### ➤ SOLAS/Ch.II-2/Reg.11 (Structural integrity)

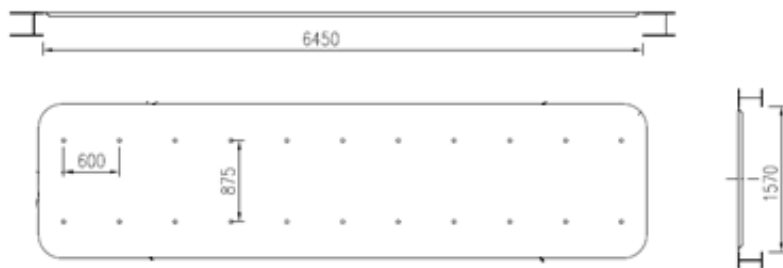
- Longitudinal and ultimate strength analysis is done without participation of composite panels, only steel part considered
- Local structural design is done to ensure that any type of cargo can hold their position in case of any composite panel failure

→ Structural integrity is fully ensured by steel members → **SOLAS compliant**

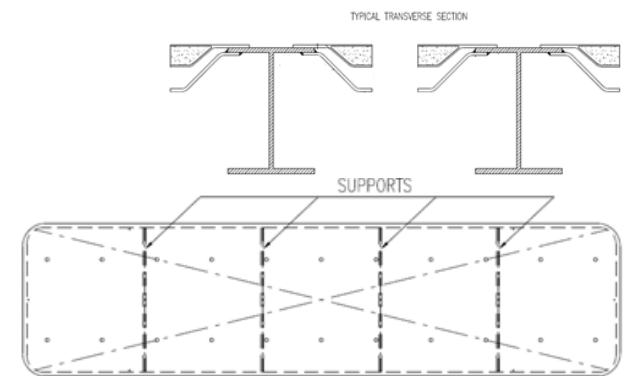
## STEEL GRILLAGE - “Composite” deck view



## COMPOSITE PANEL – covering the openings in the steel grillage



Conventional design  
procedure  
→ Additional supports



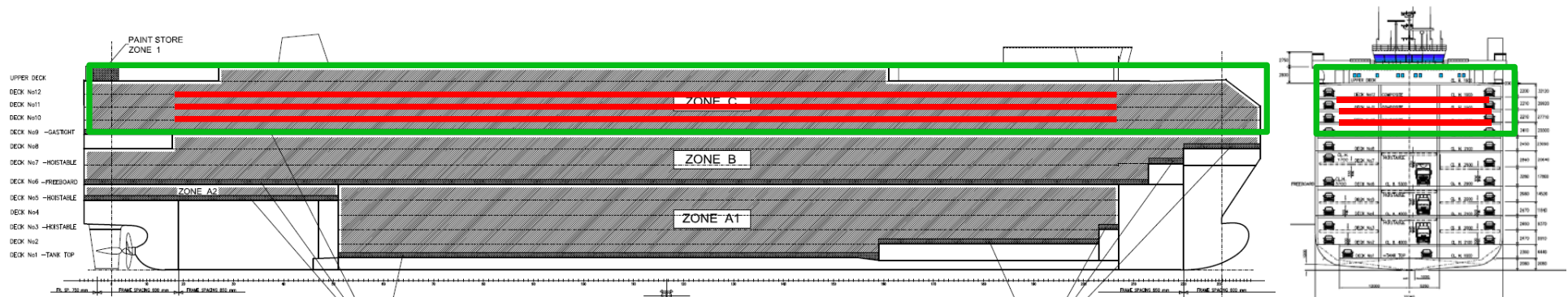
# „Composite decks” on a SOLAS vessel

## SOLAS - FIRE SAFETY

### ➤ SOLAS/Ch.II-2/Reg.9(Containment of fire)

➤ Composite decks are within same fire zone bounded by steel gastight structure → no fire protection requirements by SOLAS → **SOLAS compliant**

➤ **CLASS:** no requirement additional to SOLAS





# Design procedure

## WORK DONE ACCORDING TO RULES&REGULATIONS REQUIREMENTS

- Structure design
  - Steel grillage
  - Composite panels
- Firefighting and fire detection system
- Outfit design
  - Cargo Lashing – on the composite panel

## ADDITIONAL ASSESMENT – owner requirement, was not required by rules&regulations

- Fire safety assesment done by independent company (RISE)
  - Two HAZID workshops
  - preliminary analysis in qualitative terms
  - Large scale fire tests (steel and composite deck structure)
  - quantitative analysis – 12 FDS simulations performed (6 steel & 6 composite)
- Improvements of the deck design according to fire safety assesment results

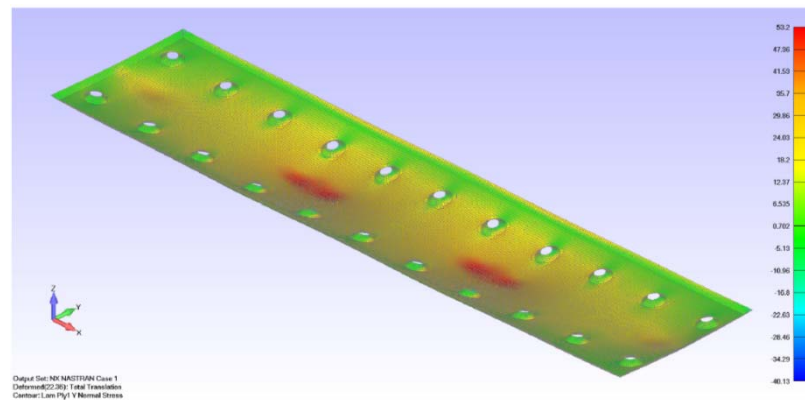
**SOLAS compliant vessel with respect to Fire safety according to SOLAS „Alternative design procedure”**

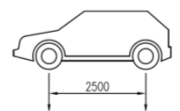
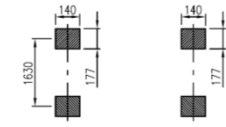
# Composite sandwich panel design

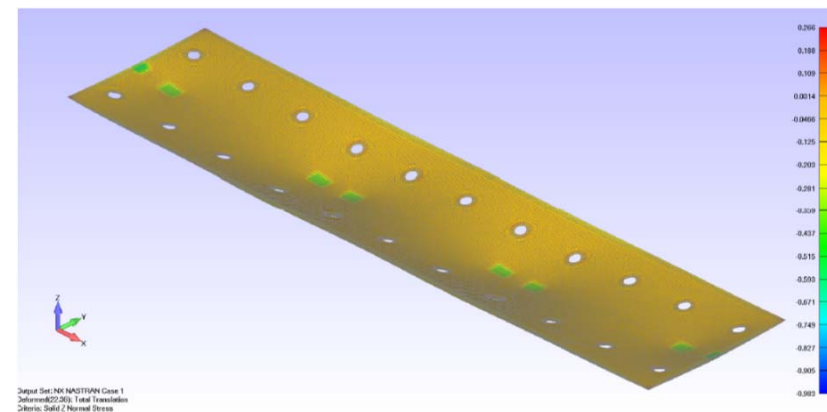
Composite sandwich panel optimisation :

- Number of glass fiber layers and fiber direction optimisation
- Core type analysis (PVC, PET, PUR)
- after selection of the core type
  - Core layout optimisation
  - different properties at specific locations (PVC80 and PVC100 used)

FEA according to BV Rules



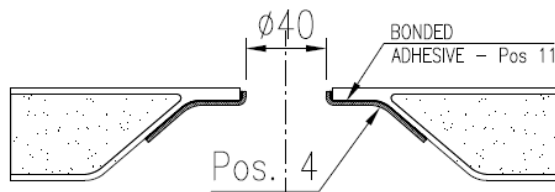
NAME	LOAD AT	AXLE LOAD (t)	TYRE PRINT (mm)	HOMOGENEOUS LOADING (t/m <sup>2</sup> )
PRIVATE CAR	SEA	L=4.8 m    B=1.9 m 		0.20



# Composite sandwich panel design

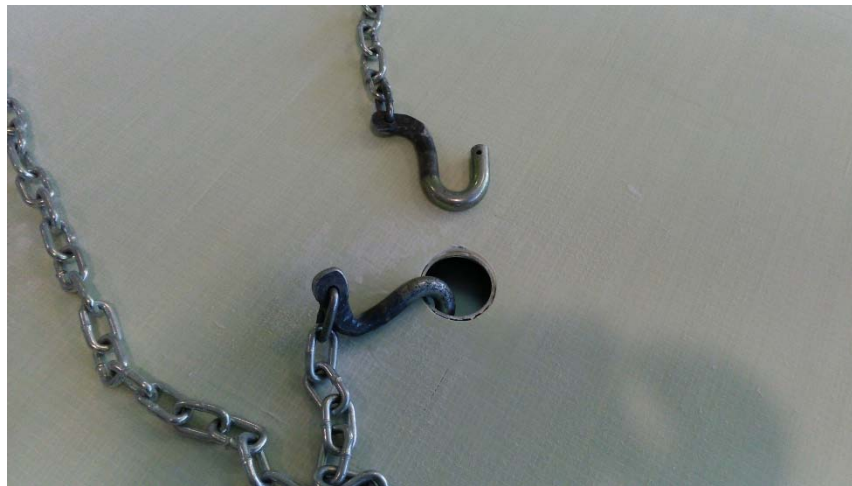
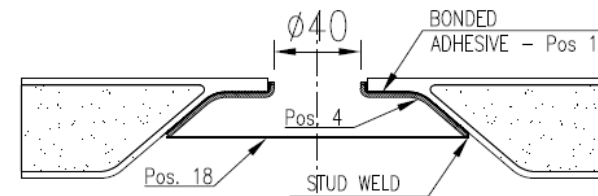
## PANEL OUTFITTING: CARGO LASHING

INITIAL VERSION



FINAL VERSION

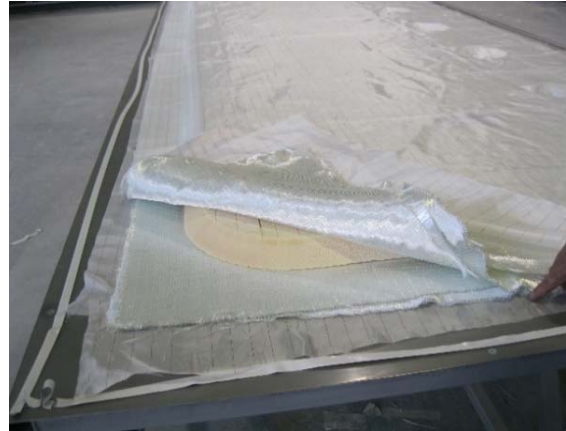
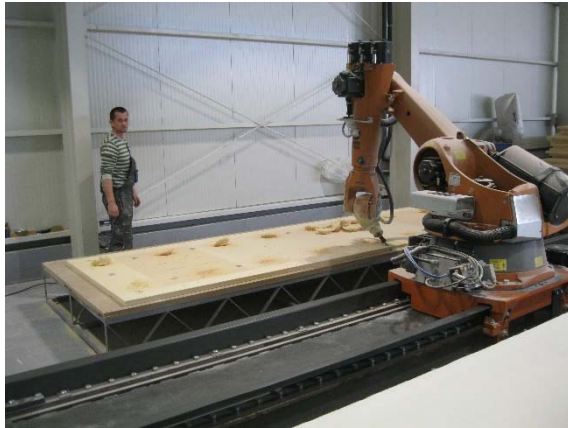
- improved according to fire test results
- lashing opening closed with steel plate



# Composite sandwich panel production

## IMPLEMENTATION ON CAR CARRIER / 7000 cars

1043 composite panels installed on three upper decks (glass fibers, PVC Core, vacuum infusion,...)





# Composite sandwich panel production



**FIBER CONTENT M=74.2 %**  
200 tests (1000 specimens)

**PANEL WEIGHT =155 kg**  
**TOTAL 162 t** (1043 pcs)





# „Composite decks” –Steel grillage production



# „Composite decks” on a SOLAS vessel



Flexible bolt  
connection

Total building  
tolerance at  
each connection

**+5 mm**



# „Composite decks” on a SOLAS vessel



- Total area covered by composite structure: **12600 m<sup>2</sup>**  
→ 2.5 football field
- Total Weight reduction of **230 t**
- Steel weight reduction of **390 t**  
→ equal to the weight of one conventional steel deck
- Improved stability performance  
→ Reduced ballast weight in double bottom tanks  
2.5x weight reduction or **575 t**

## Summary:

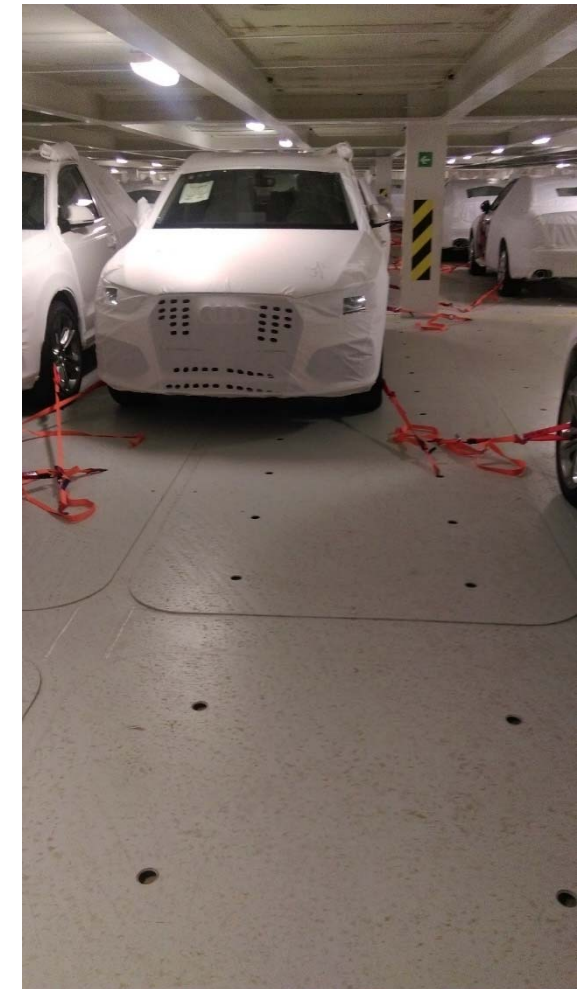
- Increased cargo intake for 230 t + 575 t = **805 t**
- Or reduced fuel consumption for **4.5% (2.1 t/day)** and CO<sub>2</sub> emissions for same cargo intake

*„lowest fuel consumption per CEU of any PCTC in its class”*

# Life cycle



# Life cycle





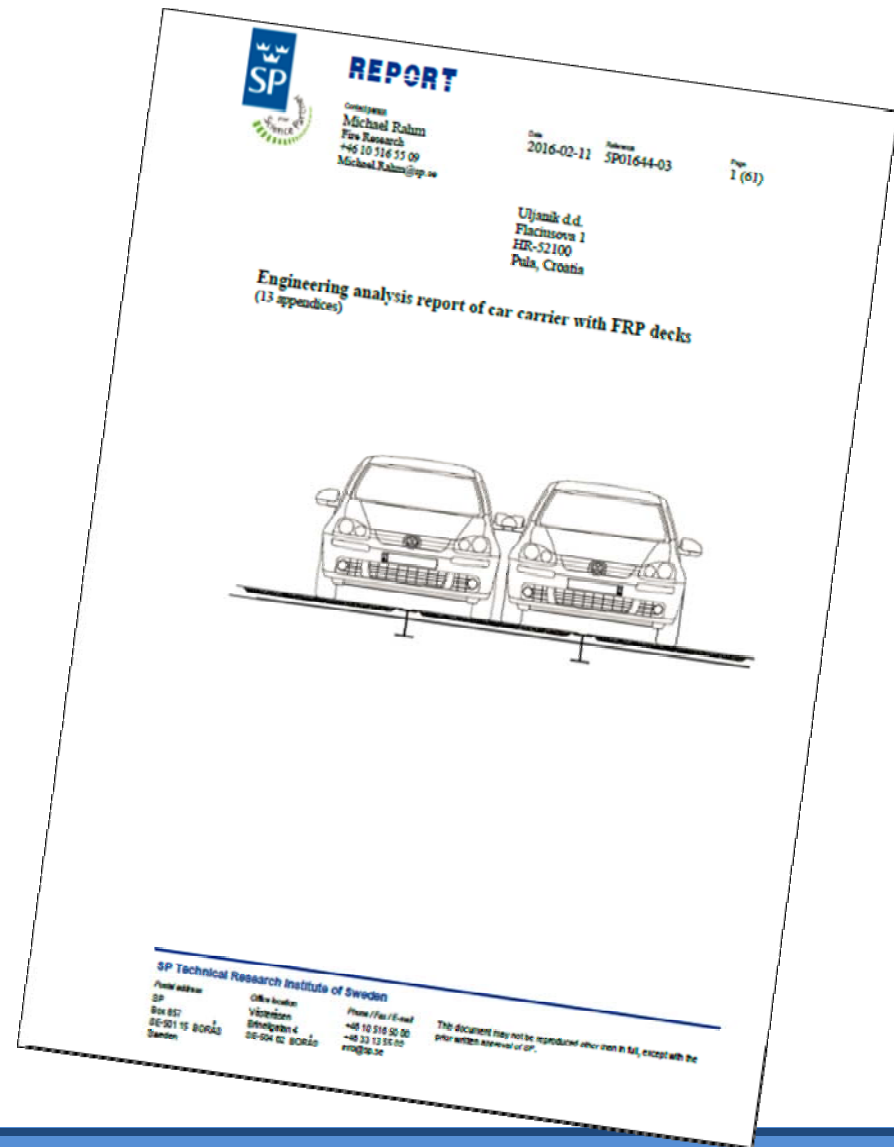
# Fire safety assessment

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# Fire safety assessment

## Fire safety assessment

- Background
- Advantages/disadvantages of the design
- Performance criteria
- Fire tests
- FDS-simulations
- Evacuation analysis
- Results



# Fire safety assessment

## Background

- Flag considered the design compliant to prescriptive requirements
- Fire safety assessment performed for further demonstration of sufficient safety
- Assessment performed according to MSC/Circ.1002

# Fire safety assessment

## Advantages/disadvantages of the design in case of fire

### Advantages

- Delayed fire spread through decks
  - Insulating material
  - Closed lashing holes delays vertical fire spread
- Escape routes can be over the panels in case of fire below deck
- Global structural integrity depends on the steel part of structure
- Cargo safety
  - Cargo Lashing functionality

### Disadvantages

- Increased fire growth rate
- increased fire load
- structural integrity of the panel
- Toxicity; burning PVC creates hydrochloride.

# Fire safety assessment

## Performance criteria

- Safe evacuation (at dock)
  - Fire risk is measured in expected fatalities due to a superstructure fire
  - One fatality = a person exposed to untenable conditions
  - Average risk presented as Expected Fatalities per Fire in gastight zone C (EFF).
- Structural integrity (at sea)
  - Probability of integrity loss and expected time is analyzed for all relevant end events.
  - The risk measure is presented as a weighted expected time to integrity loss.
  - $$\frac{1}{\sum \frac{\text{Probability of integrity loss}}{\text{Time to integrity loss}}}$$
- Containment of fire (at sea)
  - Probability of containment failure and expected time is analyzed for all relevant end events.
  - The risk measure is presented as a weighted expected time to containment failure.
  - $$\frac{1}{\sum \frac{\text{Probability of containment loss}}{\text{Time to containment loss}}}$$



# Fire safety assessment

## Fire tests

Performed to evaluate differences regarding:

- Fire growth rate
- Vertical fire spread

## Steel deck:



# Fire safety assessment

## Fire tests

Performed to evaluate differences regarding:

- Fire growth rate
- Vertical fire spread

## FRP deck:



# Fire safety assessment

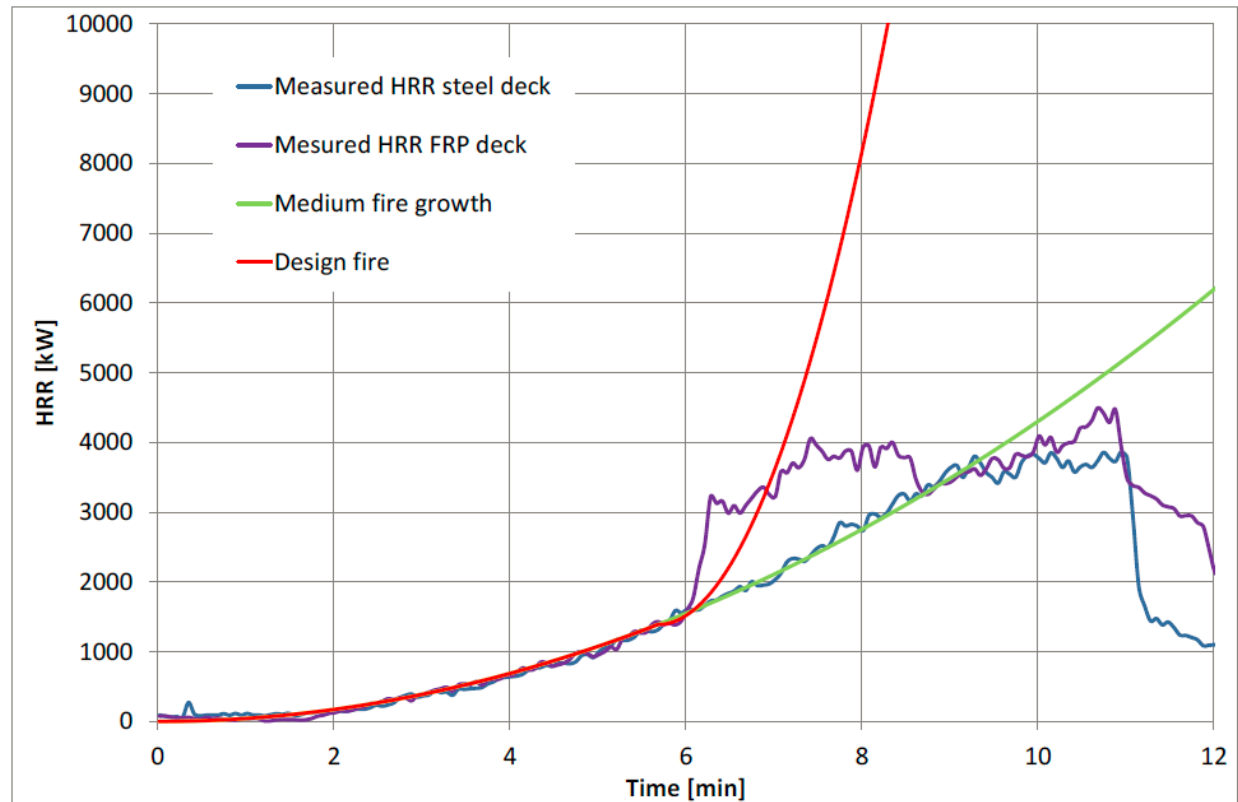
## Fire tests - Observations

Observation	Time for observation		
	Test 1, Steel	Test 2, FRP FR-coated	Test 3, FRP
Smoke from the tyres on the deck	04:54	03:54	03:26
Flames through lashing holes	08:45	04:12	05:30
Ignition of first tyre	09:41	05:22	06:06
All tyres are burning	10:21	06:26	06:09
Lashing ropes ignites	10:51	Not established	N.A.

# Fire safety assesment

## Fire tests - HRR

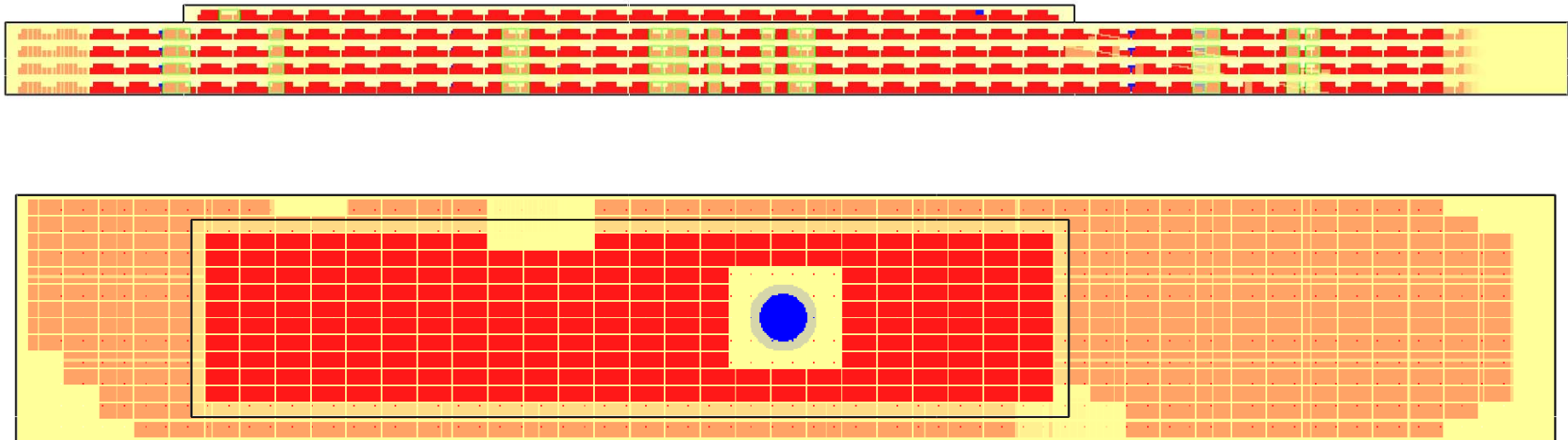
- HRR Steel deck:  
Measured HRR (oxygen consumption calorimetry) from the test with the steel deck
- HRR FRP deck:  
Measured HRR from the test with the uncoated FRP
- Medium:  
Medium fire growth, representing car fire on steel deck. Will be used as design fire in steel case in the simulations.
- Design fire:  
Based on measured HRR in these tests and earlier experience with vertical fire spread. Will be used as design fire in FRP case in the simulations.





# Fire safety assessment

## FDS Simulations – The model





# Fire safety assessment

## FDS Simulations

18 simulations were performed, varying:

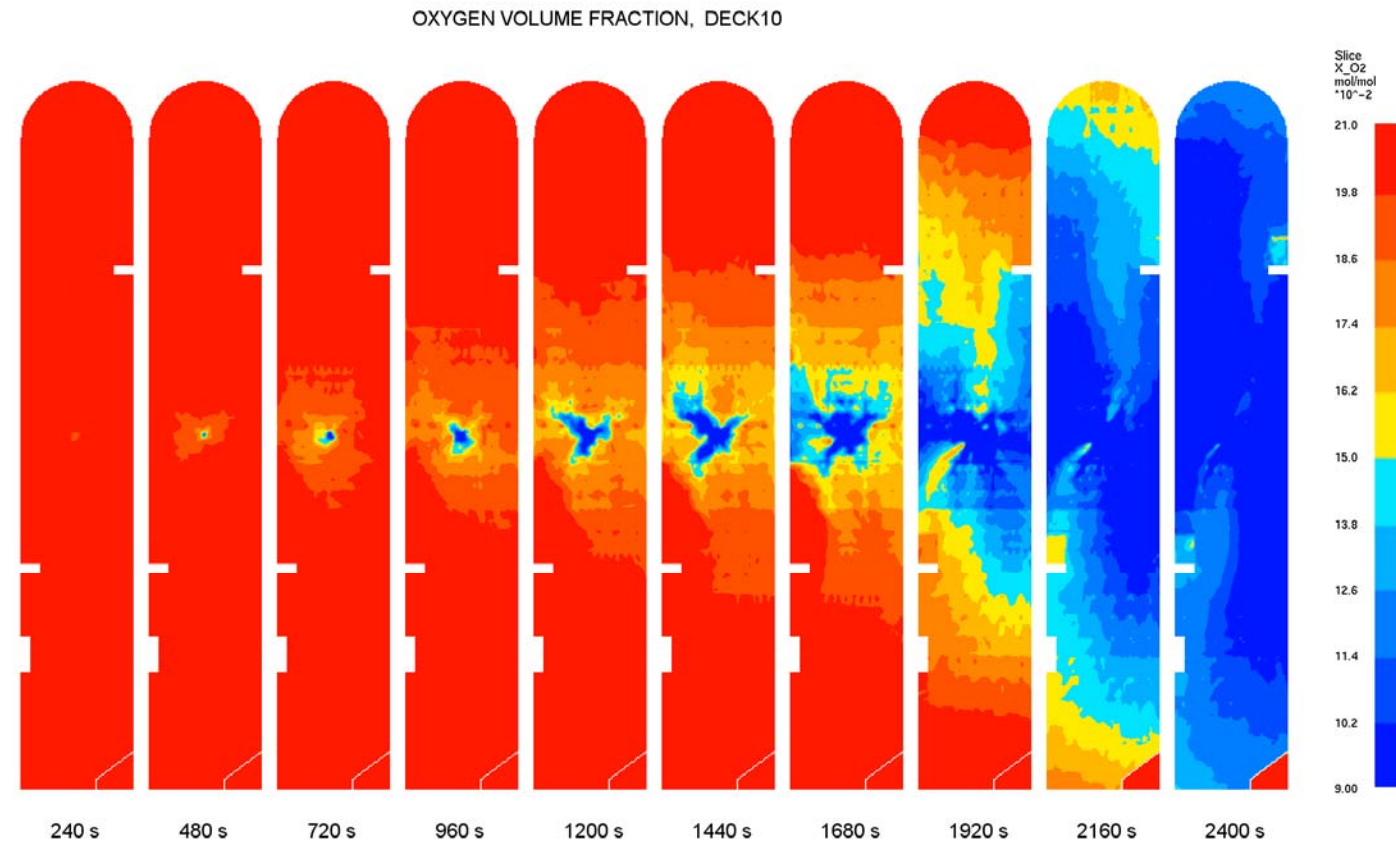
- Fire growth rate (steel/FRP)
- Ventilation conditions
  - Land/sea scenario
  - Time to close vents
- Fire origin deck
- Time to vertical fire spread (steel/FRP)

# Fire safety assessment

## FDS Simulations

### Example

- Steel design
- Land scenario
- Fire start on deck 10

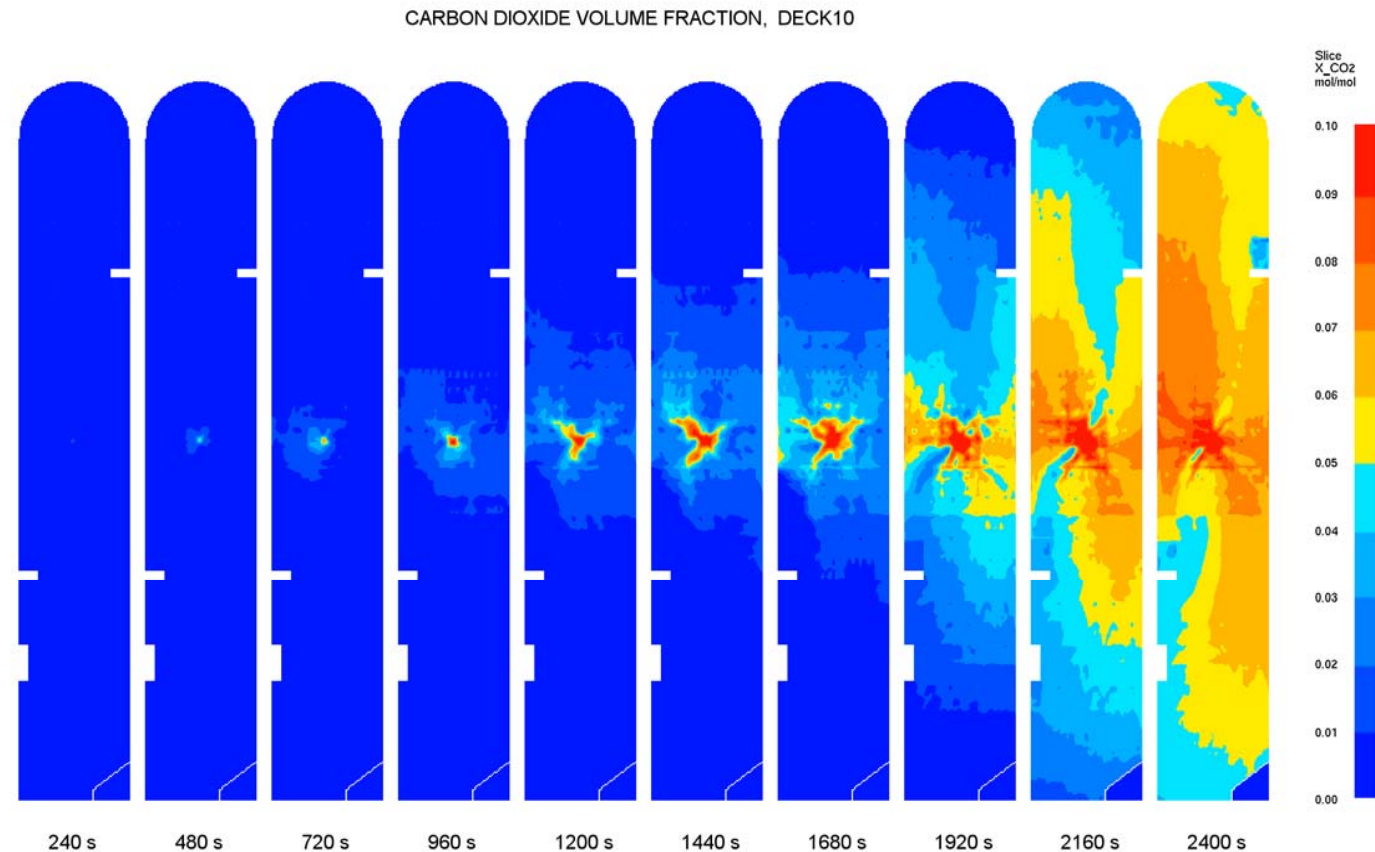


# Fire safety assessment

## FDS Simulations

### Example

- Steel design
- Land scenario
- Fire start on deck 10

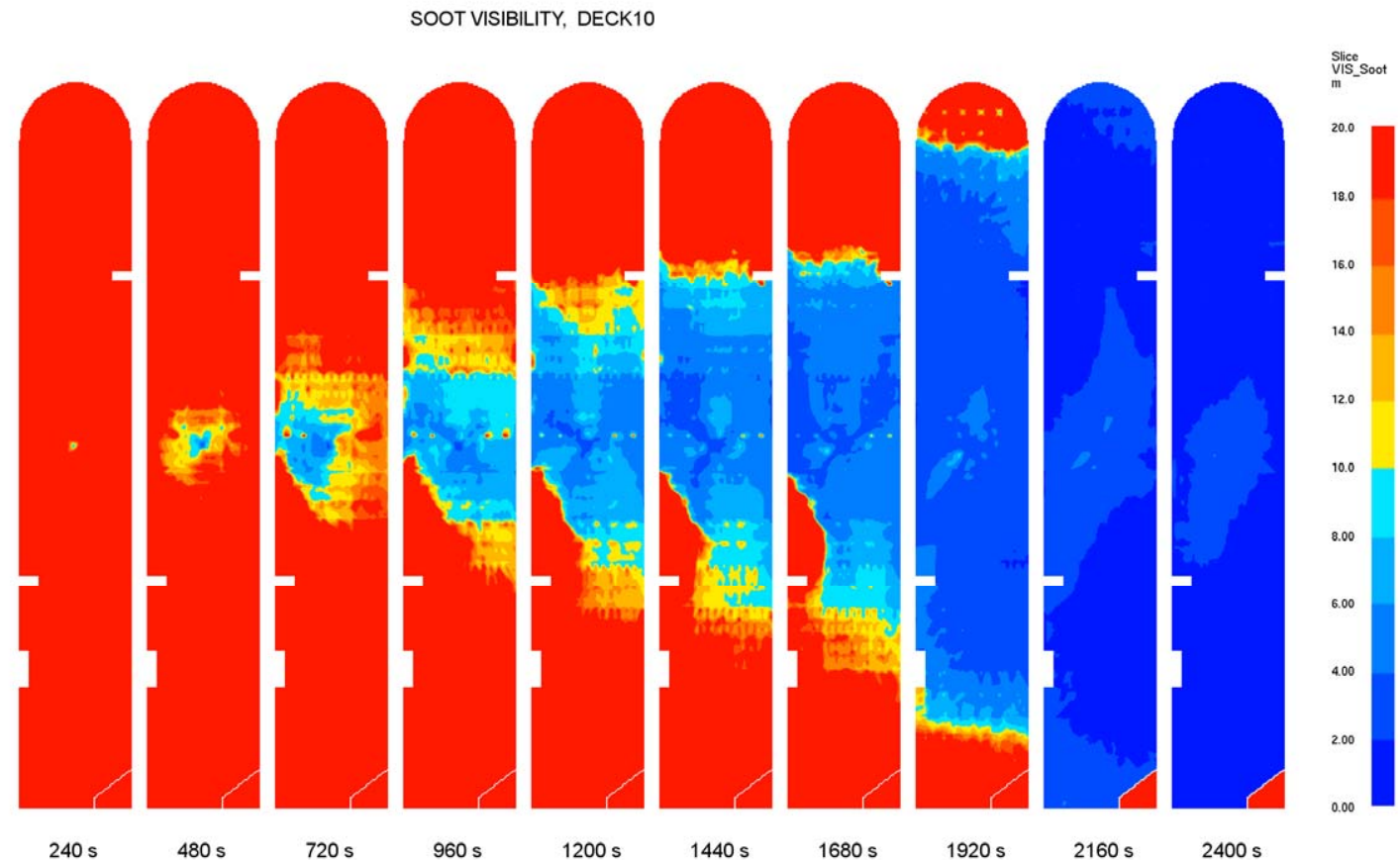


# Fire safety assessment

## FDS Simulations

### Example

- Steel design
- Land scenario
- Fire start on deck 10

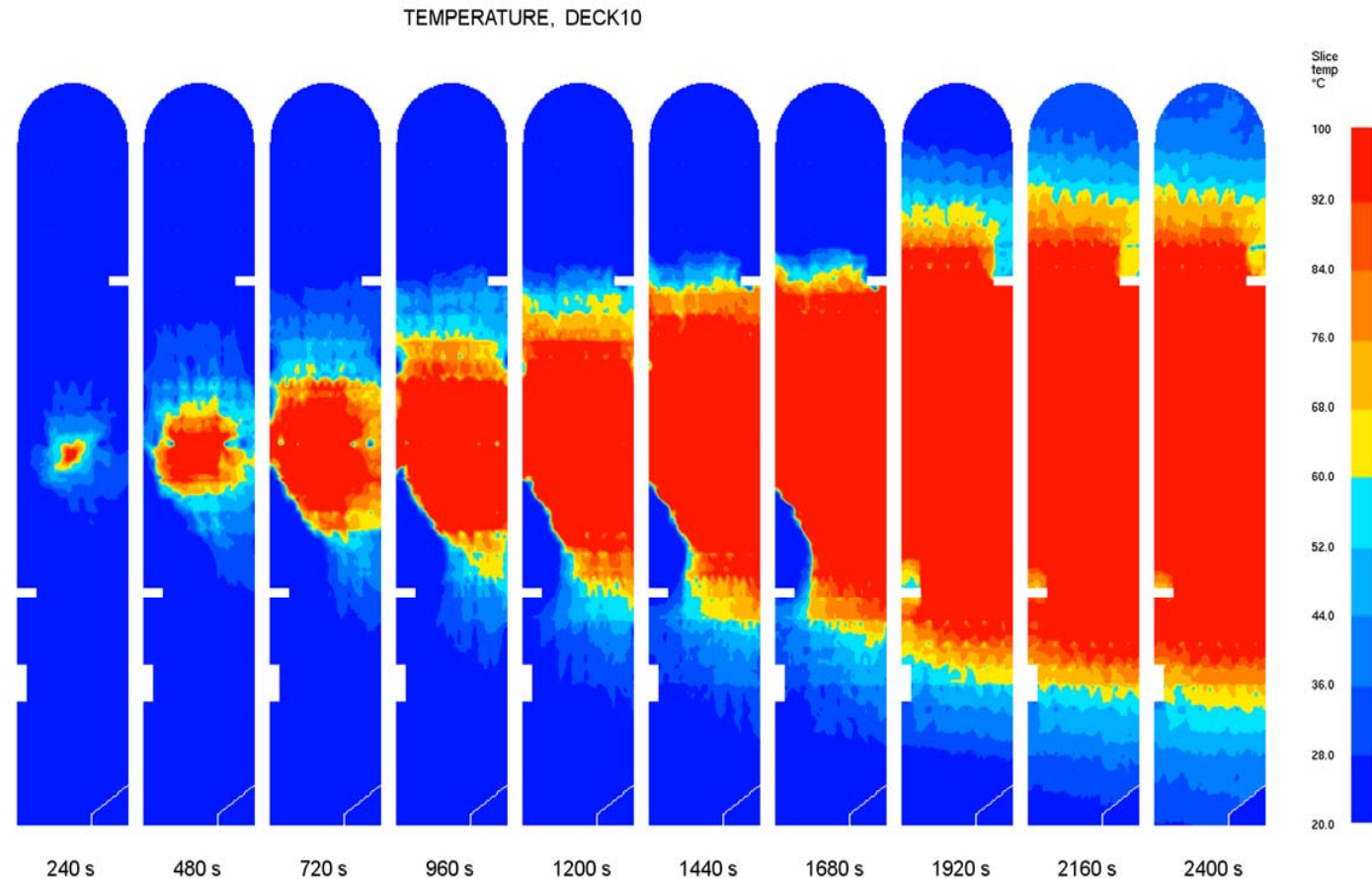


# Fire safety assessment

## FDS Simulations

### Example

- Steel design
- Land scenario
- Fire start on deck 10

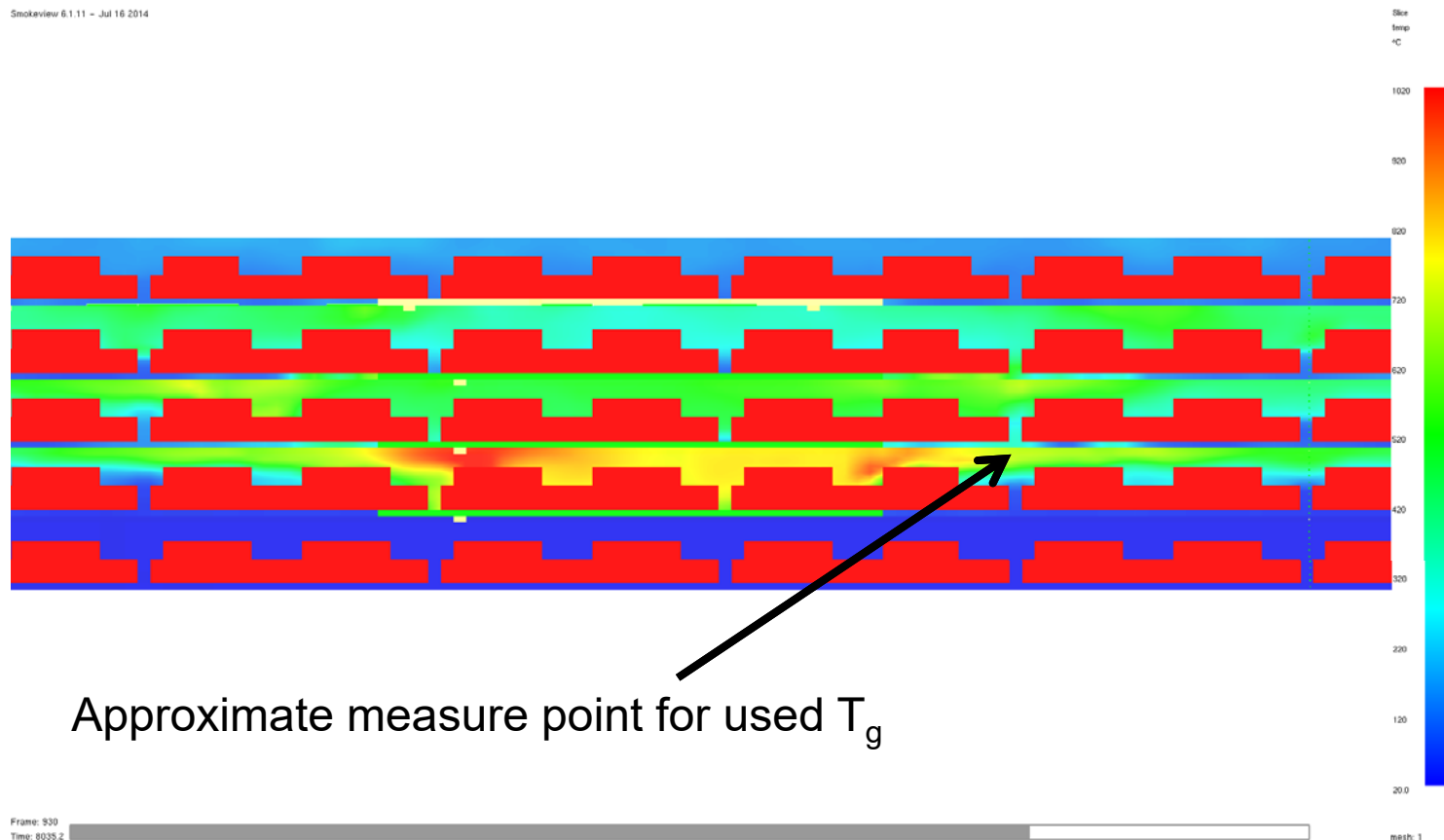




# Fire safety assessment

## Steel beam temperatures

- Gas temperatures taken from CFD simulations 40 cm above and below the deck closest to the fire.
- Homogene steel temperature.

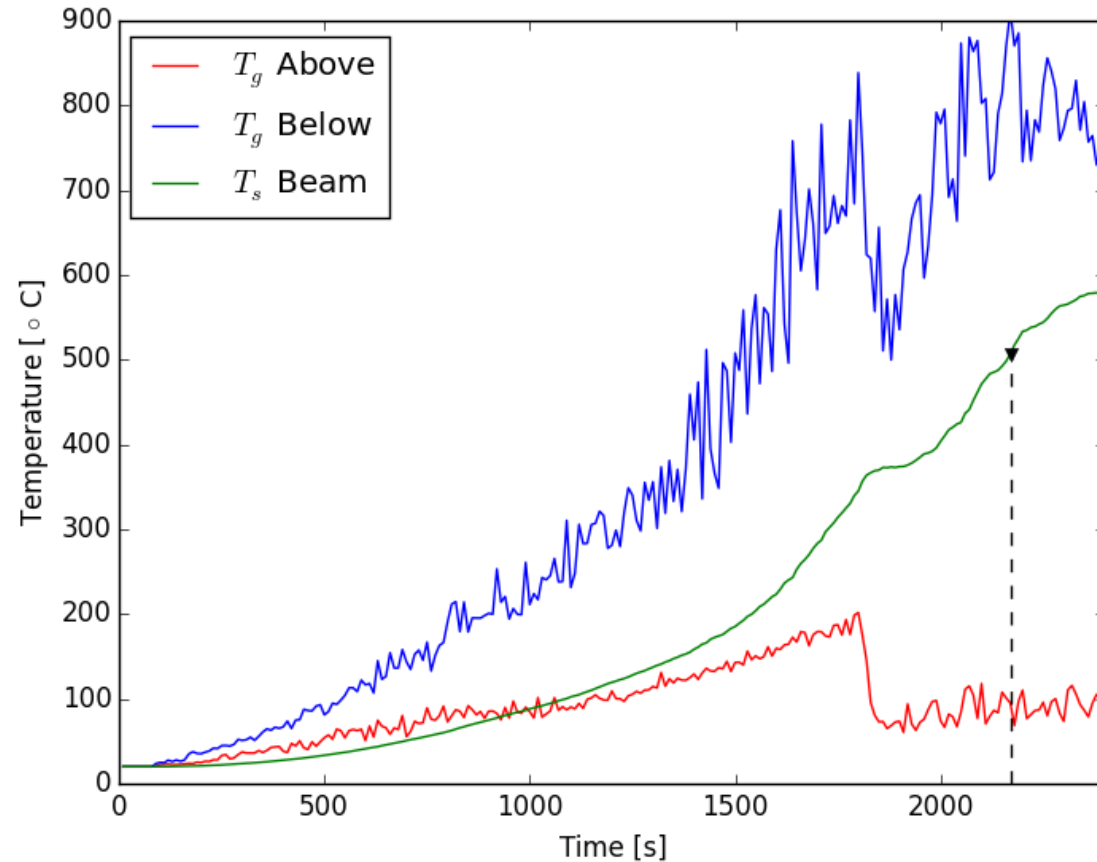


# Fire safety assessment

## Steel beam temperatures

### Example

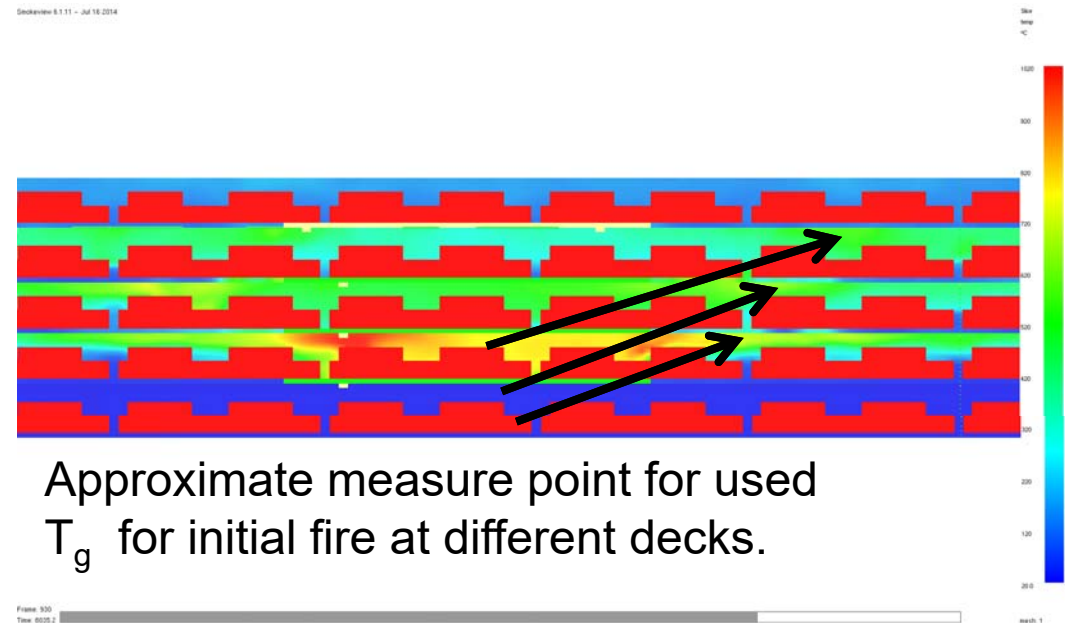
- Steel design
- Land scenario
- Fire start on deck 10



# Fire safety assesment

## Fire spread to accomodation

- Gas temperatures taken from CFD simulations 40 cm below the deck right above, 2 decks above, and 3 decks above the initial fire.
- Fire spread is assumed to happen when  $\Delta T = 140^{\circ}\text{C}$  which means  $T=160^{\circ}\text{C}$ .
- Material properties for worst possible A30 deck used.
- No cooling on top of deck.

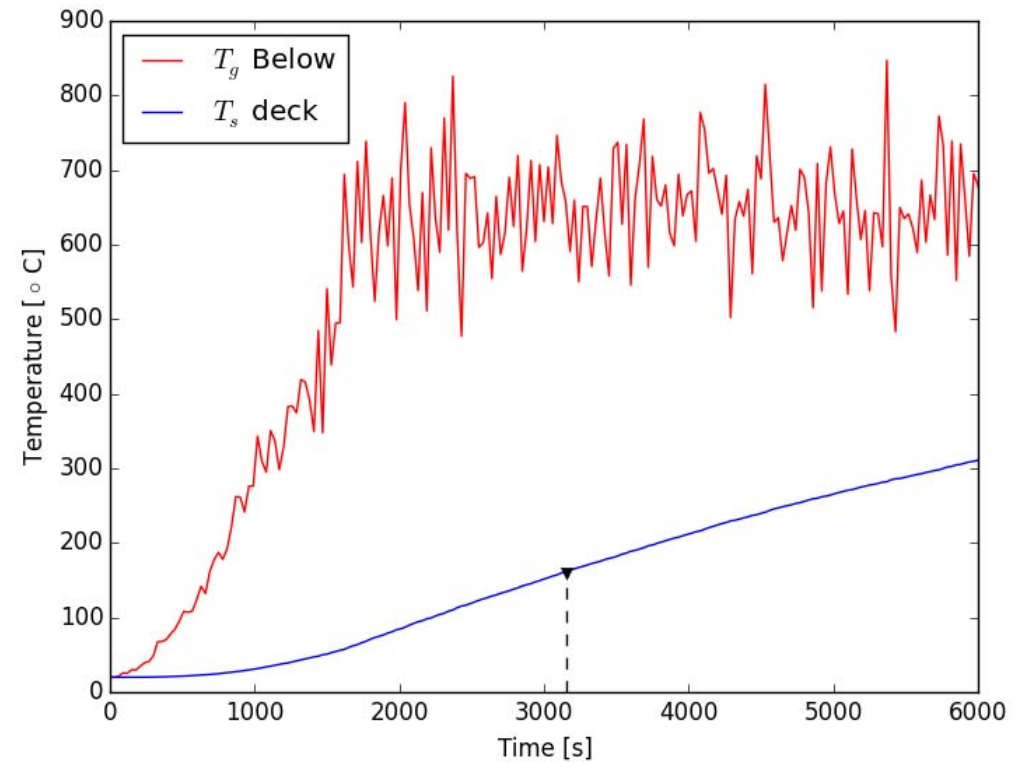


# Fire safety assesment

## Fire spread to accomodation

### Example

- Steel design
- Vents not closed
- Fire start on deck 12



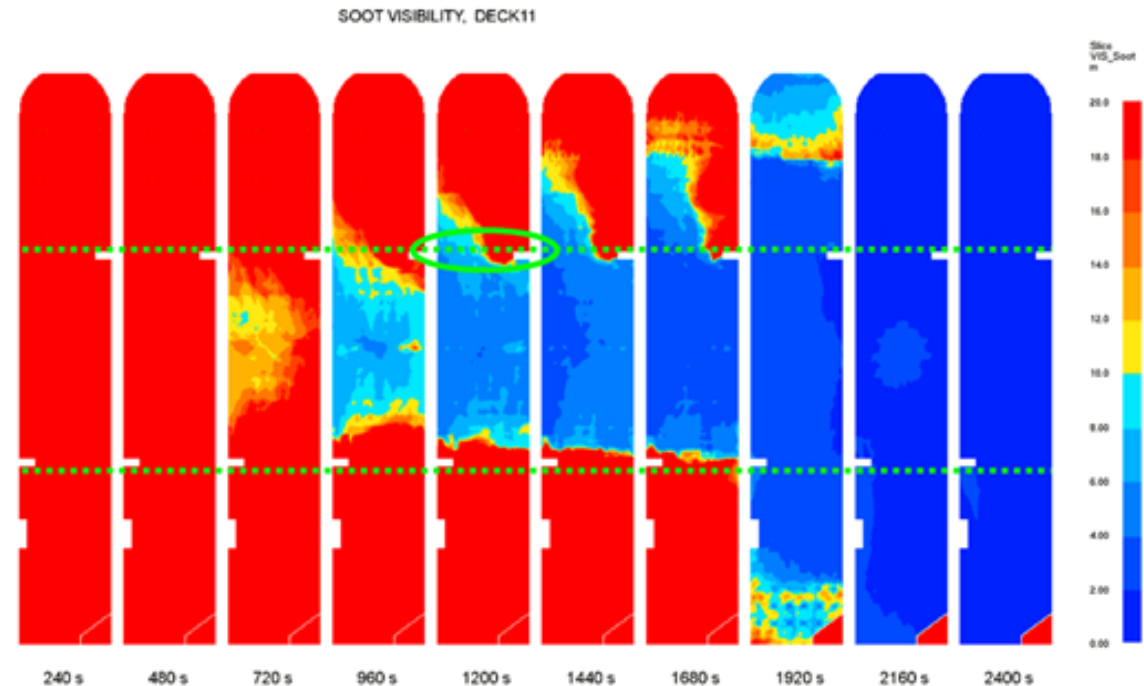
# Fire safety assessment

## Evacuation analysis

$$ASET - RSET > 0$$

ASET = Available Safe Egress Time:

- Time to untenable conditions in a compartment:
  - Visibility: 1,8 m above floor level the visibility must be more than 10 m.
  - Temperature: max 60°C
  - Toxicity: 1,8 m above floor level:
    - CO > 1400 ppm
    - CO<sub>2</sub> > 5 %
    - O<sub>2</sub> < 15 %
    - HCL > 1000





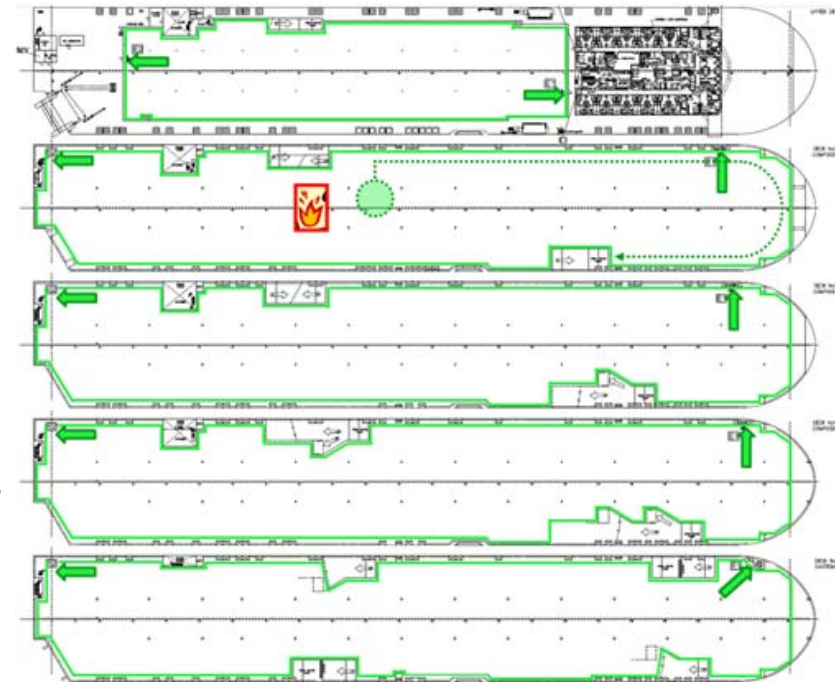
# Fire safety assessment

## Evacuation analysis

$$ASET - RSET > 0$$

RSET = Required Safe Egress Time:

- RSET (evacuation time)=recognition time + response time + movement time
  - Recognition time: 1-10 min depending on detection, position (what deck) and alertness
  - Response time: 1-5 min depending on detection, alertness, and if actual fire signatures are observed.
  - Moving time: 0.6 m walkways along ship side. 150 m distance (see fig). 1.2 m/s (corridors according to MSC/Circ.1033). ->2 minutes walking time



# Fire safety assessment

## Results

Criteria	Prescriptive design	Base design
PLL	0	0
Expected safety margin	20.5 min	13.5 min
Probability of structural integrity failure	12 %	51 %
Probability of loss of containment	10 %	10 %
Weighted average time to structural integrity failure	418 min	31 min
Weighted average time to containment failure	706 min	597 min

# Fire safety assessment

## Trial alternative design 2

- New lashing hole design
  - Prolonged vertical fire spread
  - Fire spread to deck below (burning droplets) eliminated
  - Cargo lashing functional for longer time in fire scenario
- Automatic/remote controlled dampers
  - Fast closing (immediately after alarm); fire is ventilation controlled before structural damage and containment loss.
  - Reduced probability of failure (automatic functionality + manual effort in case of failure)
  - Faster CO<sub>2</sub>-activation
- Position feedback on doors and dampers
  - Allows crew to focus on failing doors and dampers
  - Reduces risk of CO<sub>2</sub> activation despite failing doors and dampers
- A30 insulation below lifeboat embarkation station
  - Allows safe lifeboat embarkation in case of uncontrolled fire in Gastight zone C

# Fire safety assessment

## Results

Criteria	Prescriptive design	Base design	TAD2*
PLL	0	0	0
Expected safety margin	20.5	13.5	13.5
Probability of structural integrity failure	12 %	51 %	3 %
Probability of loss of containment	10 %	10 %	1 %
Weighted average time to structural integrity failure	418 min	31 min	552 min
Weighted average time to containment failure	706 min	597 min	5973 min

\*In addition: safer embarkation, earlier CO<sub>2</sub>-activation (less damaged cargo)



# Conclusion

## **SOLAS compliant vessel with composite structure:**

- Deck structure weight reduction of 25% (230 t)
- Increased cargo intake for 805 t or fuel consumption reduction of 4.5% (2.1 t/day HFO) for same cargo intake
- Production cost and lead time
- Improved safety of cargo in case of fire
- Improved safety of crew in case of fire below deck with respect to Escape routes

## **SOLAS compliant vessel with respect to Fire safety according to SOLAS „Alternative design procedure”**

# Further development at RAMSSES (WP14)

Project full title: **Realisation and Demonstration of Advanced Material Solutions for Sustainable and Efficient Ships** (Grant agreement No.: **723246**)

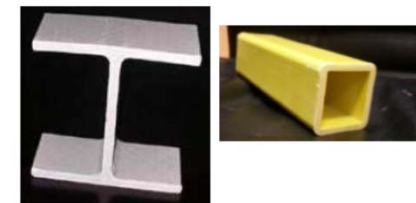


ULJANIK YARD 513 (Car Carrier 7000 cars) - to be used as base design where :

- -FRP structure design using the technology of Pultrusion
  - as a replacement of the sandwich composite panel
  - as a replacement of the sandwich composite panel and steel supporting structure
  - Combination of profiles and sandwich panel



**Expected improvements:** Improved flexibility in the design process, Production cost and lead time reduction, Joints development, Modular assembly of Composite components on board the ship



# Contacts

Contacts and questions welcome at:

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