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MARITIME

Numerical simulation for thermo-mechanical analysis within alternative design

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Introduction & Motivation

- Fibre reinforced plastic (FRP) is an interesting material for maritime industries because of:
 - weight-strength relation (reduced structural weight),
 - efficient fabrication of complex shapes (moulding freedom),
 - low affinity of corrosion etc.
- Usage of FRP is limited by its fire behaviour, i.e. typically in fire FRPs tend to react exothermic and loose their form stability
- As a consequence, the usage of FRPs in ship building is limited by current regulations, e.g. to:
 - Parts permitted to have lower fire resistance
 - Ship types with limited service range (-> High Speed Craft)
- Only possibility for using FRPs in other areas: demonstrate <u>safety equivalence</u>!

IMO Alternative Design (MSC.1Circ.1455, 2013)

Introduction & Motivation

- Important characteristics to be considered for demonstrating safety equivalence
 - Smoke
 - Toxicity
 - Fire resistance / flammability
 - SOLAS functional objectives
 - 1.1 The fire safety objectives of this chapter are to:
 - .1 prevent the occurrence of fire and explosion;
 - .2 reduce the risk to life caused by fire;
 - .3 reduce the risk of damage caused by fire to the ship, its cargo and the environment;
 - contain, control and suppress fire and explosion in the compartment of origin; and
 - provide adequate and readily accessible means of escape for passengers and crew.
- For complying with this functional objective
 - Temperature conductivity needs to be limited (controlled)
 - Bulkhead needs to be intact as a fire barrier

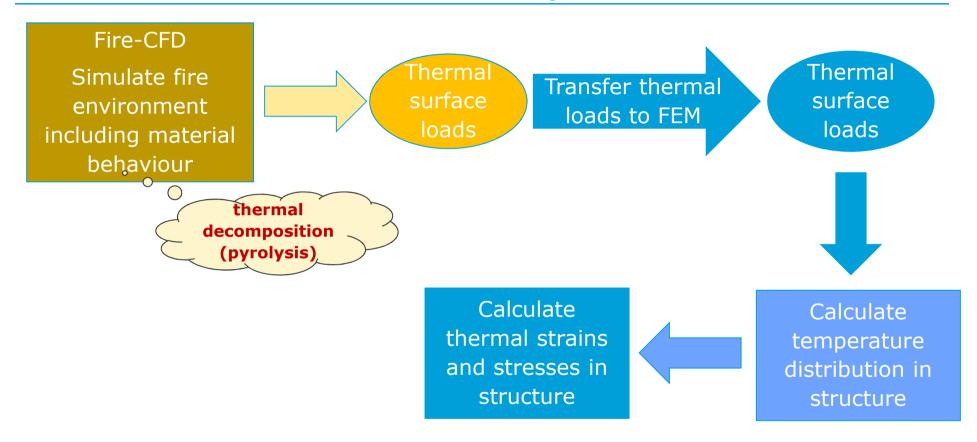
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Fire-Resist

- EU project in FP 7 2011 2015 by
- Partners: ACG, AMORIM, AP&M, APC, BAL, Bombardier, EADS, FSG, Gaiker, INSA, Proplast, SICOPM, SP, Steinbeis R-tech, VTT
- Selected objectives
 - Develop new reinforced plastic materials with increased fire resistance
 - Develop tools for <u>numerical simulation</u> of structural fire behaviour
- Numerical simulation allows
 - Detailed investigation of the behaviour of structures in fire, e.g.
 - Temperature distribution
 - Thermal strains and stresses
 - Remaining load bearing capacity

Thermo-Mechanical Simulation Concept

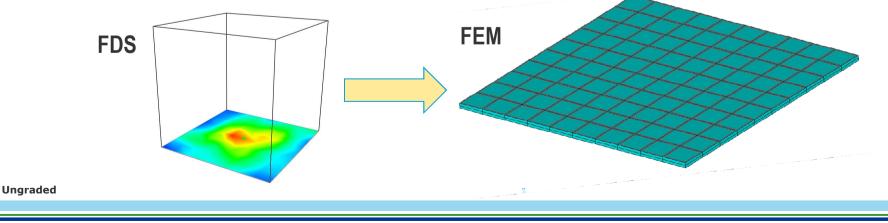


Fire Simulation

- Simulation carried out using Fire Dynamic Simulator (FDS)
 - Coupled sub-models for calculating
 - Fluid dynamics
 - Gas phase chemical reactions
 - Radiation
 - Solid phase heat conduction
 - Pyrolysis -> central role in the simulation of combustible materials
- For simulation of FRPs, needed parameters
 - Directly measured
 - If not possible: small scale test, e.g. kinematic parameters for approximating temperature dependent rate of thermal decomposition were determined via thermo-gravimetric analysis (measure the mass loss and heat release rate)

Thermo-Mechanical Analysis

- Finite Element technique offers the possibility to solve the thermo-mechanical problem, i.e. temperature distribution and related strains
- Typically for problems with negligible small heat release by mechanical deformation => one-directional coupling (thermal -> mechanical)
 - Calculate time dependent temperature field in the structure based on the thermal loads determined by FDS
 - Calculate thermal strains and related stress considering also other external loads if any
- For this process: Routine developed for mapping FDS thermal loads to FE model (ANSYS and ABAQUS)

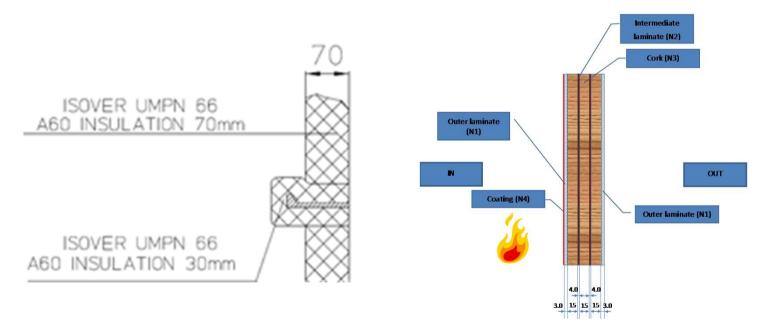


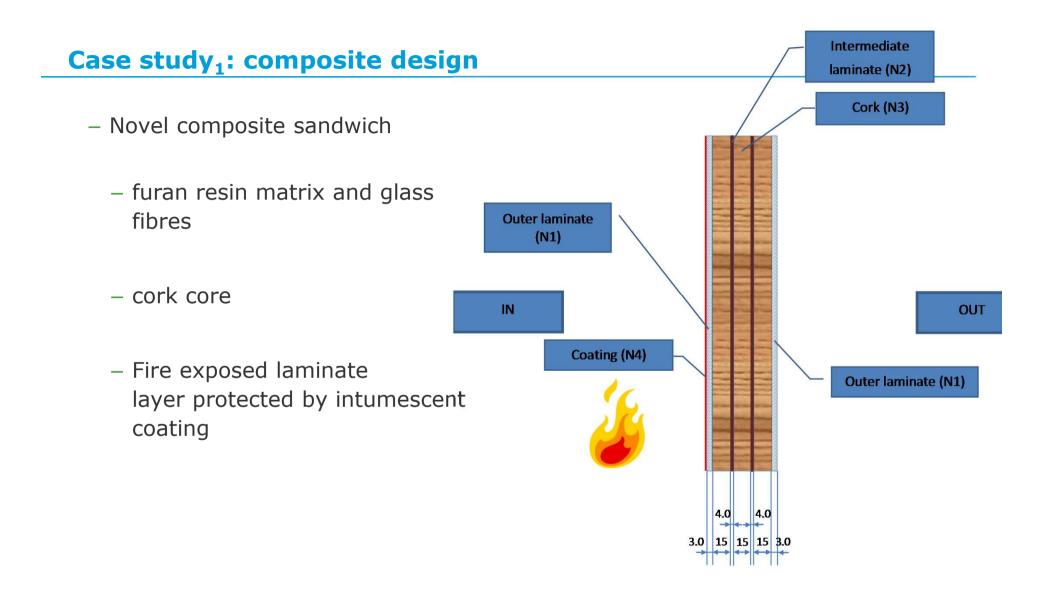
Proposed concept

- Part/ wall of Ro-Ro cabin
- Wall with A-60 class equivalence
- The wall/ cabin element was further investigated in two possible designs:
 - Using steel and insulation
 - Using novel composite materials

Case studies: reference and novel design

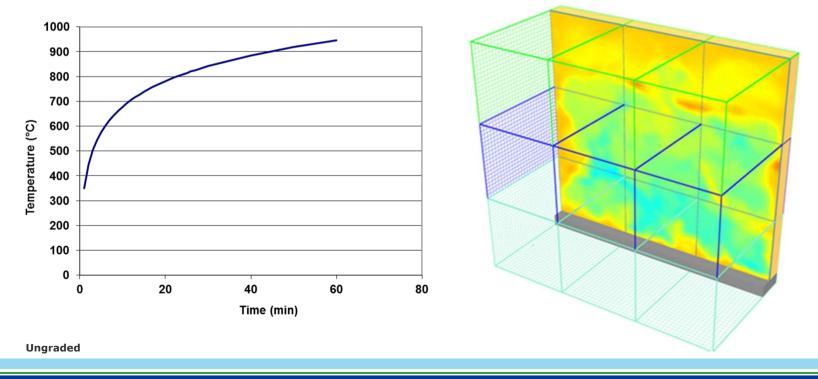
- Comparative thermo-mechanical analysis was carried out for a typical bulkhead of A-60 Class:
 - Following test requirements of FTP Code
 - Traditional steel (1) and novel composite (2) solutions





Case study₂: Fire Simulation

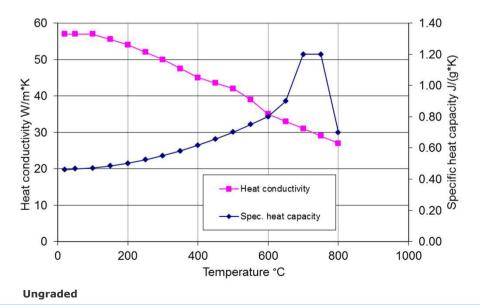
- Fire simulation using Fire Dynamics Simulator (FDS)
- Furnace walls follow ISO 834 time-temperature curve
- The FDS model considers eight air inlets and eight air outlets of 100 mm × 100 mm, volume flow is 50 l/s
- Furnace size is 2950 mm × 1500 mm × 3000 mm with 50 mm mesh resolution



Case study₃: material properties modelling

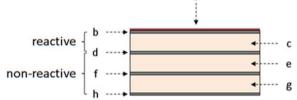
Steel

- Temperature dependent properties
 - Thermal conductivity
 - Specific heat capacity
 - Thermal expansion
 - Yield strength



Composite

Reactive material for first two layers



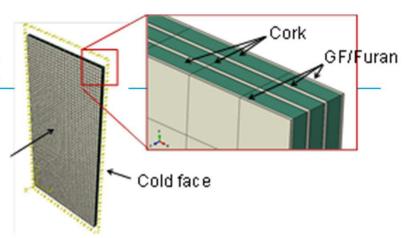
- Intumescent coating is modelled as a 50 mm thick, non-reactive, layer of material with a Furan laminate: three step decomposition reaction
- 2nd & 3rd cork layer: temperature dependent thermal conductivity and specific heat capacity
- All other layers: constant thermal conductivity and specific heat capacity

Case study₄: composite material model

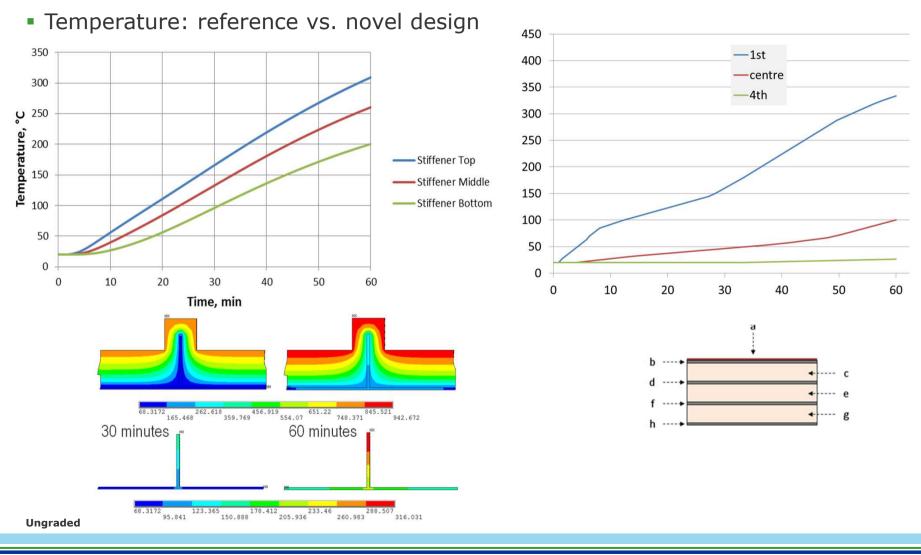
- Composite
 - For mechanical FEA
 - Linear elastic behaviour assumed
 - Temperature dependent properties for
 - Cork
 - Modulus decreases from 15 MPa (RT) to 5 MPa (150°C)

Hot face

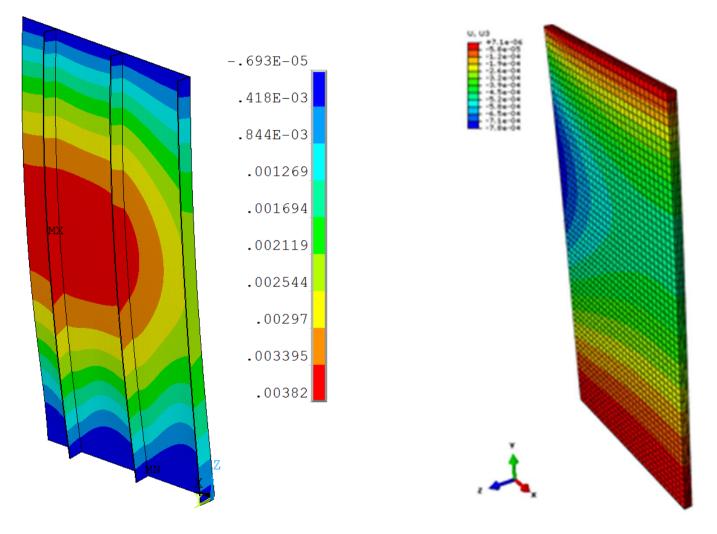
- Composite
 - Mori-Tanaka homogenisation scheme has been used to estimate composite unidirectional (UD) ply properties



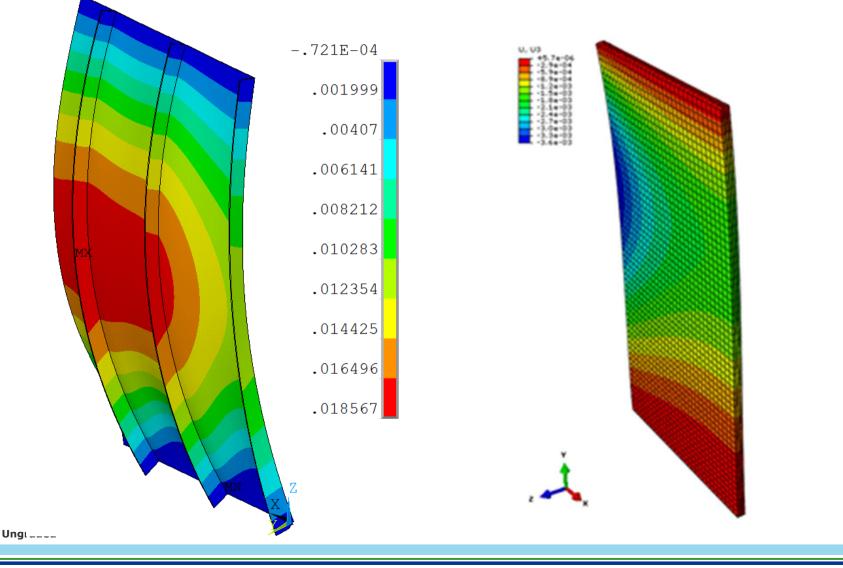
Results₁: thermal calculation



Results₂: horizontal deflection for ~15 min (magnitude x 20)



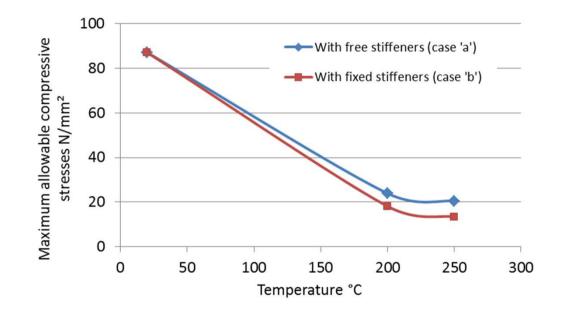
Results₃: horizontal deflection for ~60 min (magnitude x 20)



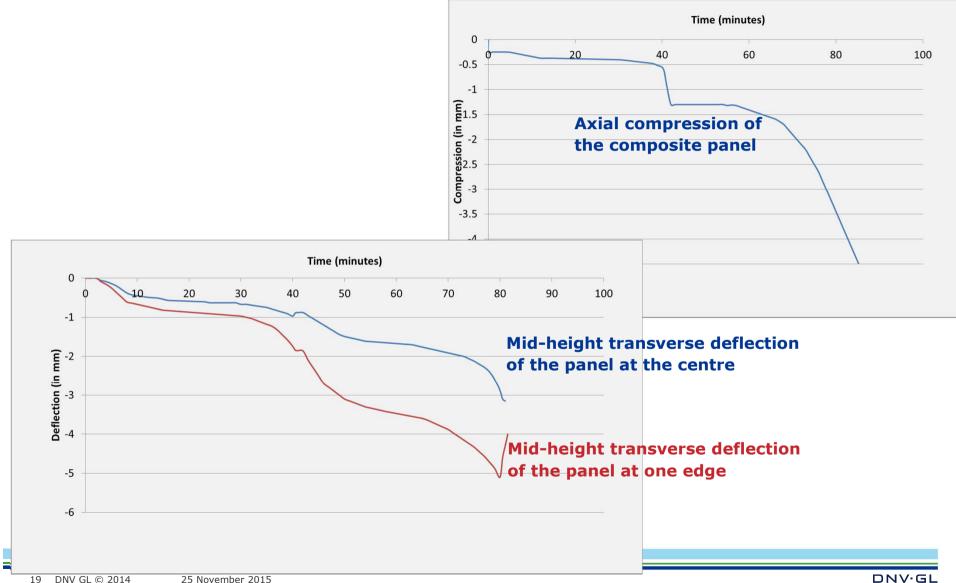
Results₄: mechanical results for steel design after 60 min

von Mises stresses (N/mm²)

load-bearing capacity (based on DIN-18800-3) using deflections and stresses from ANSYS calculation



Results₅: mechanical results for composite design after 60 min



Comparison based on numerical results after 60 min fire exposure

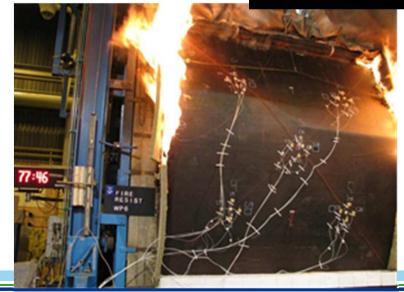
Criterion	Insulated steel bulkhead	Composite bulkhead
Average temperature rise on unexposed side (requirement ≤ 140°C)	137°C	≤ 5°
Maximum temperature rise on unexposed side (requirement ≤ 180°C)	183°C (fulfilled considering numerical uncertainty)	≤ 5°C
Load bearing capacity	25 N/mm ²	2.1 N/mm ²
Relative loss of load bearing capacity	71%	~95%
Structural integrity (keep fire in compartment of origin)	Fulfilled: The bulkhead keeps its structural integrity but experiences significant load-bearing capacity reduction. It still has structural reserves (29% of the initial state or 25 N/mm ² in terms of stresses)	structural integrity. (*) However, the load-bearing limit is reached and no more structural reserves

Fire test (performed at SP)

- A fire test was performed in order to
 - Verify the simulation process for composite material
 - Demonstrate the capabilities of the materials developed in Fire-Resist

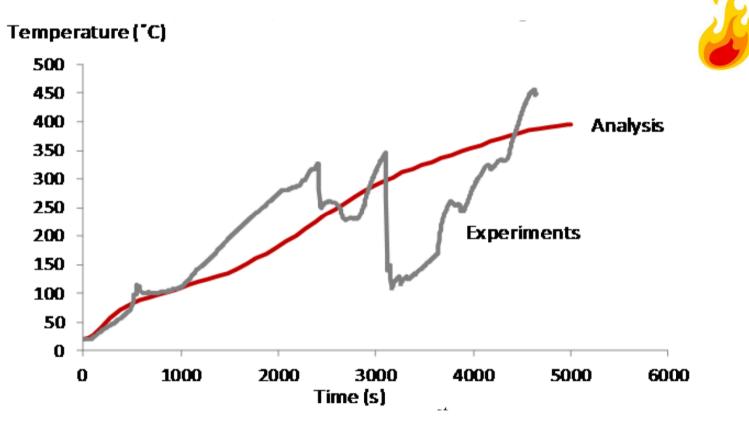






Comparison between 1st laminate temperatures measured during the test and simulated with the FEA (test data: SP)

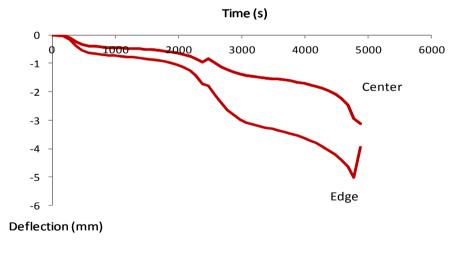
 Comparison between 1st laminate temperatures measured during the test and simulated with the FEA

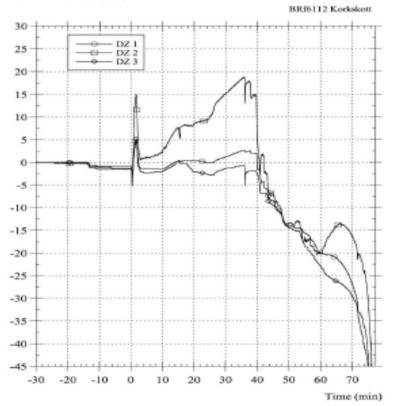


Comparison: measured and simulated horizontal deflection of the composite bulkhead (test data source: SP)

Horizontal deflection (mm)

- The trend of the curves is very well predicted
- A time of a first instability predicted at 40 min
- Final collapse predicted starting at 65 min





Summary & Conclusion

- Usage of composite materials in shipping industries limited
- Possibility to overcome limitations: IMO Alternative Design
- Thermo-mechanical analysis can help
 - To analyse the behaviour of structural elements during and after a fire
 - Optimise the design in order to
 - Meet the functional objectives required by regulations
 - Minimise experiments
 - To comparatively analyse novel and reference materials with respect to their fire behaviour
- In Fire-Resist a concept for numerical fire simulation and subsequent thermomechanical analysis was developed
- This concept is based on FDS fire simulation and allows thermo-mechanical analysis using ANSYS or ABAQUS

Summary & Conclusion

- This concept was exemplarily applied to a bulkhead made of two different materials:
 - Traditional steel insulated
 - Novel composite consisting of cork and furan laminate protected by intumescent coating
- The results demonstrate the capabilities of this concept providing an excellent possibility for detailed analysis of structural fire behaviour

Thank you for your kind attention

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