



TECHNICAL REPORT – TR 06-08 r3

Title: Design of Panel for Fire Testing according to IMO Res MSC45(65)	
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Customer/	LÄSS
Application/	Marine
Country:	Sweden

Department: TS	Project no:
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Background

In the LASS project a typical deck panel and bulkhead that has a DNV approved design shall be tested in a fire test according to IMO Res. MSC 45(65). The lay up of the panels are described in this document together with calculations for the DNV approval.

Geometry

Attached drawings:

"Outline dimensions fire test panel.dwg"

Span between supports = 3300 mm, (Total length is 3425 mm)

Span between stiffeners = 2000 mm (Total width is 3200 mm)

The stiffeners have a height 200 mm and a with (core thickness) of 50 mm.

Load

Deck Panel Static Pressure

Pressure = 350 kg/m^2

Area = $3.3 \times 4 = 13.2 \text{ m}^2$

Total load = $350 \times 13.2 = 4620 \text{ kg}$

Load for each "load distribution beam" = $4620/2 = 2310 \text{ kg}$

Bulk Head

In the fire test a vertical line load of 700 kg/m will applied on the upper edge.

Since the bulkhead is water tight it also needs to be designed to take a Uniform Load of 13 kN/m^2 . This load case is controlled in the calculations.

Temperature

The insulation is designed (se document?) so the panel and the stiffeners will not be exposed to a temperature above 80 C° . Hence the panel shall be designed for a temperature of 80 C° for 1 hour.

Manufacturing Method:

The panels and stiffeners will be manufactured with infusion in one step.

Sandwich Lay Up

The panel is made with Divinycell foam and E-glass fibre/polyester laminates. The thickness values given for the glass fibre laminas in the tables below are approximate values, since the thickness will varies with the actual volume fraction fibre, typical is 44-48 % (64 % by weight) for an infused laminate.

Deck Panel

Table 1. Lamina in the Deck Panel. *Estimated thickness.

Material	Weight [g/ m ²]	Thickness* [mm]
GF Biaxial 0/90	1600	1,36
Divinycell H80		50
GF Biaxial 0/90	1200	1,02
Total thickness, mm		52,38

Table 2. Lamina at the sides of the stiffener. *Estimated thickness.

Material	Weight [g/ m ²]	Thickness* [mm]
GF Biaxial 45/-45	3*800	2,04
Divinycell H80		50
GF Biaxial 45/-45	3*800	2,04
Total thickness, mm		54,4

Table 3. Lamina at the bottom of the stiffener. *Estimated thickness.

Material	Weight [g/ m ²]	Thickness* [mm]
GF Biaxial 45/-45	800	0,68
GF Uni Directional	600	0,51
GF Biaxial 45/-45	800	0,68
GF Uni Directional	600	0,51
GF Biaxial 45/-45	800	0,68
GF Uni Directional	600	0,51
Total thickness, mm		3,57

In the fire test panel, the stiffener shall be reinforced at the four support points. The reinforcement starts at the end of the stiffeners and is 200 mm long. The reinforcement is made by switching the core H80 to H250 and increasing the glass fibre lamina with 2400 g/m² Biaxial 0/90 that is wrapped around the edge and all the way up to the panel

Bulkhead

Table 4. Lamina in the Bulkhead. *Estimated thickness.

Material	Weight [g/ m ²]	Thickness* [mm]
GF Biaxial 0/90	1200	1,02
Divinycell H80		50
GF Biaxial 0/90	1200	1,02
Total thickness, mm		52,04

Material Properties

Table 1. *Estimated Material properties: Divinycell H80 at 80 C.*

Material	Density	E-modulus	G-modulus	Shear Strength
H80	80 kg/m ³	32.5 MPa	11.5 MPa	0.45 MPa

Table 2. *Estimated Material properties: Glass fibre/Polyester laminates at 80 C.*

Fibre skins

Designation	Fib/Res Ratio	Tens. str. [MPa]	Comp. str. [MPa]	Tens. mod. [MPa]	Comp. mod. [MPa]	Flex. mod. [GPa]	Th. factor [mm/kg/m ²]
E-Glas Biax (0/90)	1,66	400	320	17000	17000	17	0,85
E-glas D-biax (+/-45)	1,66	400	320	17000	17000	17	0,85
E-glas Uni (0)	1,66	650	350	30000	30000	30	0,85

Deck panel - Static pressure load



SUMMARY OF RESULTS		
Design object: Deck panel "LASS"		Date: 06.02.2006
Customer:		Designer:
DESIGN		PROPERTIES
Resin:	Iso polyester	Outer skin thickness: 1,36 mm
Process:	Vacuum bagged	Inner skin thickness: 1,02 mm
Adhesive:		Total thickness: 52,38 mm
Designation	Layer W/T Unit	Panel weight: 9,15 kg/m ²
E-Glas Biax (0/90)	1600 g/m ²	Panel cost: /m ²
Divynycell H80(min) a 80 gr.	50 mm	Flexural rigidity: 26,303 Nm ² /mm width
E-Glas Biax (0/90)	1200 g/m ²	

SANDWICH / LAMINATE		
PROPERTIES		
Laminate thickness	Outer skin	1,36 mm
	Inner skin	1,02 mm
	Total thickness	52,38 mm
	Laminate weight	9,15 kg/m ²
	Flexural rigidity	26,303 x10 ⁶ Nmm ² /mm width
	Shear stiffness	0,603 x10 ³ N/mm width
If the outside skin is in compression failure is expected in the	skin at a moment of	6,253 x10 ³ Nmm/mm width
If the outside skin is in tension failure is expected in the	skin at a moment of	4,753 x10 ³ Nmm/mm width
	Maximum shear load	23,04 N/mm width

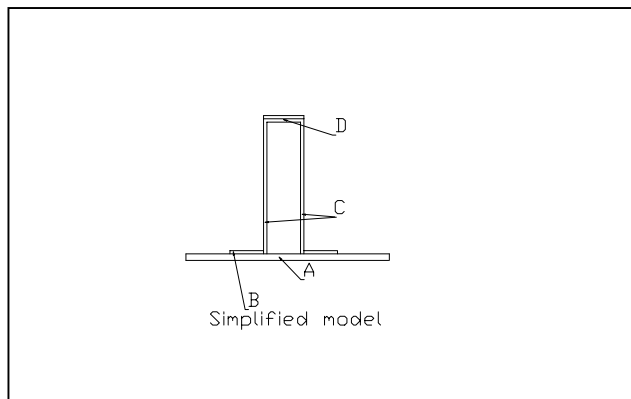
PANEL BENDING: SIMPLY SUPPORTED PANEL

Panel length	3200 mm	Midpanel deflection	18,55 mm
Panel width	2000 mm	Shear deflection	13,4 %
		Bending ratio L/	107,8
Panel pressure	3,5 kN/m ²	Safety factor at center of panel	5,2
		Safety factor at end of panel	N/A
		Shear stress	0,059 N/mm ²
		Safety factor for shear	7,7

Deck stiffener - Static pressure load

Deck panel, "LASS", Section modulus requirements for stiffeners										
Pt. 3, Ch.4, sec.7-fig.1										
								Sigma ultimate		
								400	Mpa	
					Rules			Sigma		
		Factor	p	l	b	Max M	fig. 1	(Mpa)	Required	
Stiffener	Position	C1	(kN/m2)	(m)	(m)	(kNm)	b eff	* 0.3	Z cm3	Stiffener type
DEKK										
Stiver		8	3,5	3,2	2	9,0	300	120	75	

Calculation of top hat stiffeners:



Ref	Part	t (mm)	b (mm)	A (mm2)	z (mm)	Az (mm3)	Az2 (mm4)	I (mm4)
A	Bottom (eff.)	1,1	300	330	0,55	181,5	100	33
B	In-lamination	2,04	100	204	2,1	432	917	71
C	Web laminate	200	4,08	816	101,1	82497,6	8340507	2720000
D	Flange laminate	3,57	60	214,2	202,885	43457,967	8816970	227
	Summary			1564,2		126570	17158494	2720332

Neutral axis from bottom: 80,9 mm (n.a. 1)

Neutralaxis from flange 119,1 mm (n.a. 2)

I 9637264 mm4 963,7 cm4

Z 80929 mm3 80,9 cm3 (n.a. 2)

Z 119101 mm3 119,1 cm3 (n.a. 1)

Bulk Head – Uniform Pressure 13 kN/m²

Design object: Bulk head "LASS"			Date: 2006-02-06		
Customer:			Designer:		
DESIGN			PROPERTIES		
Resin:	Iso polyester		Outer skin thickness:	1,02 mm	
Process:	Vacuum bagged		Inner skin thickness:	1,02 mm	
Adhesive:			Total thickness:	52,04 mm	
Designation	Layer	W/T	Unit	Panel weight:	8,48 kg/m ²
E-Glas Biax (0/90)		1200	g/m ²	Flexural rigidity:	23,402 Nm ² /mm width
Divynycell H80		50	mm		
E-Glas Biax (0/90)		1200	g/m ²		

Shear stiffness	1,614	x10 ³ N/mm width
If the outside skin is in compression failure is expected in the outside skin at a moment of	8,879	x10 ³ Nmm/mm width
If the outside skin is in tension failure is expected in the inside skin at a moment of	8,879	x10 ³ Nmm/mm width
Maximum shear load	51,02	N/mm width

PANEL BENDING: 50% FIXED PANEL		OWN WEIGHT NOT INCLUDED	
Panel length	2650 mm	Midpanel deflection	51,20 mm
Panel width	2440 mm	Shear deflection	6,7 %
		Bending ratio L/	47,7
Panel pressure	13 kN/m ²	Safety factor at center of panel	3,2
		Safety factor at end of panel	4,5
		Shear stress	0,222 N/mm ²
		Safety factor for shear	4,5

Comment:

Room temperature material properties for the core has been used in this calculation.

The safety margin for fibre failure is 3.2 (requirements 3.3), however the difference is very small hence the amount fibre is kept at 1200 g/m² which is the minimum requirement. The same discussion applies the L/50 requirement which here is L/47.

The reason for keeping the amount of fibre to 1200 g/m² is that the fire test shall be a worst case scenario (which it is due to the quite large panel size) with a smaller panel size the requirements above would have been fulfilled.

Bulk Head – Vertical Load 700 kg/m

A buckling calculation has been made in ESAComp.

Plate buckling and FPF

Laminate : H80 50 mm - 1200 g 0/90 h = 52.04 mm

Plate: a = 2650 mm; b = 2440 mm;

Laminate load : $N_y = -7000$ N/m

Factor of safety : $FoS^v = 1$

Stability factors : $SF_g = 1$, $SF_1 = 1$

Failure crit. (reinf.;core) : Max stress;Von Mises

Buckling load

$N_x = 0.00$ N/m $\sigma_x = 0.00$ MPa $\epsilon_x = 0.0083$ %

$N_y = -37240.00$ N/m $\sigma_y = -0.72$ MPa $\epsilon_y = -0.0958$ %

$N_{xy} = 0.00$ N/m $\tau_{xy} = 0.00$ MPa $\gamma_{xy} = 0.0000$ %

Margin to failure

$MoS_{buckling} = 432$ %

$MoS_{buckling}/FPF = 432$ % Mode: Global buckling Crit. layers: -